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Interim Report For The Upper Mississippi River - Illinois Waterway System Navigation Study





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Upper Mississippi River - Illinois Waterway System Navigation Study ENV Report 5 August 1998

Physical Forces Study, Clark's Ferry, Mississippi River

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Preface

The work reported herein was conducted as part of the Upper Mississippi River-Illinois Waterway (UMR-IWW) System Navigation Study. The information generated for this interim effort will be considered as part of the plan formulation process for the System Navigation Study.

The UMR-IWW System Navigation Study is being conducted by the U.S. Army Engineer Districts of Rock Island, St. Louis, and St. Paul under the authority of Section 216 of the Flood Control Act of 1970. Commercial navigation traffic is increasing, and in consideration of existing system lock constraints, will result in traffic delays that will continue to grow into the future. The system navigation study scope is to examine the feasibility of navigation improvements to the Upper Mississippi River and Illinois Waterway to reduce delays to commercial navigation traffic. The study will determine the location and appropriate sequencing of potential navigation improvements on the system, prioritizing the improvements for the 50-year planning horizon from 2000 through 2050. The final product of the System Navigation Study is a Feasibility Report, which is the decision document for processing to Congress.

The work was performed by personnel of the Coastal and Hydraulics Laboratory (CHL), U.S. Army Engineer Waterways Experiment Station (WES) during 1995-1998. The study was under the direction of Dr. James R. Houston, Director, CHL; Mr. Charles C. Calhoun, Jr., Assistant Director, CHL; and Mr. C. E. Chatham, Jr., Chief of the Navigation and Harbors Division (NHD), CHL. The study was conducted by Drs. S. T. Maynord and S. K.Knight, both of the Navigation Branch, NHD.

At the time of publication of this report, Director of WES was Dr. Robert W. Whalin, and the Commander was COL Robin R. Cababa, EN.

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1 Introduction

Background

The Upper Mississippi River-Illinois Waterway System (UMR-IWWS) Navigation Study evaluates the justification of providing additional lockage capacity at sites on the UMR-IWWS while maintaining the social and environmental qualities of the river system. The system navigation study is implemented by the Initial Project Management Plan (IPMP) outlined in U.S. Army Corps of Engineers (1994). The IPMP outlines engineering, economic, environmental, and public involvement plans.

The environmental plan identifies the following: significant environmental resources on the UMR-IWWS; impacts to threatened and endangered species; water quality; recreational resources; fisheries; mussels and other macroinvertebrates; waterfowl; aquatic and terrestrial macrophytes; and historic properties. The plan considers the system-wide impacts of navigation capacity increases, while assessing potential construction effects of improvement projects. The physical forces studies are part of the environmental plan.

Physical Force Objectives

According to the IPMP, the objectives of the physical forces studies are as follows:

- *a.* Use Illinois State Water Survey (ISWS) field data to calibrate and validate the physical model.
- b. Increase density of measurements to refine their spatial distribution.
- c. Make a range of measurements which could not be made in the field.
- d. Expand measurements to different cross sections.
- e. Carry out statistical data analyses.

- *f.* Develop models by combining existing field data with new data developed from the physical model.
- g. Evaluate the feasibility of developing numerical solutions.

Scope of Report

The Clark s Ferry site was one of two sites used in the physical model to achieve the physical force objectives outlined above. The first experimental site was at Kampsville on the Illinois River and is referenced in this report. Specifically, the Clark s Ferry site study evaluated the far field velocities and drawdown induced by underway tows. Far field refers to all areas except those beneath and immediately adjacent to the tow. The Clark s Ferry study provides physical force data and an understanding for developing analytical models.

2 Prototype Clark s Ferry Section

Prototype Data Collection

The ISWS collected physical data on the hydrodynamic changes associated with tow and barge traffic movement on the Upper Mississippi River System. These data were collected from both the Illinois and Mississippi Rivers. The detailed report on the Clark s Ferry prototype experiments is given in Bhowmik, Soong, and Xia (1994).

The Clark s Ferry site is located at River Mile 468.2 in a relatively straight reach as shown in Figure 1. The prototype measurement site is in Pool 16, approximately 18 km (11 miles) upstream of the dam. Like many areas of the Upper Mississippi River, Clark s Ferry has submerged dikes located about 300 m apart. The dikes in the Clark s Ferry reach are angled upstream and located on the left descending bank. A reconnaissance trip, before the actual field data collection, gathered information on site characteristics, bathymetry, cross-sectional profiles, discharge, suspended sediment, and bed materials. The actual field data collection trip included collecting data on ambient conditions and during an event. Data were taken for three periods: (a) pre-passage, (b) actual passage, and (c) post-passage. Trip 1 field data were collected for seven consecutive days (May 16-22, 1991), and trip 2 for four consecutive days (October 17-20, 1991). Trip 1 was conducted during an intermediate flow period and trip 2 was conducted during a low flow. Figures 2 and 3 show cross sections for trips 1 and 2, respectively.

Prototype Instrumentation

Instrumentation used for data collection were: (a) five interocean current meters (model S4's), (b) two Marsh McBirney (MMB) 527 velocity meters, (c) six MMB511's, and (d) one wave gauge. The instruments were placed in the experimental reach for data collection. Velocity data in both the x- and y- directions were sampled at one sample per second. Positive x velocities were downstream and positive y velocities were toward the left bank. Wave data were sampled at 10 samples per second.

For trip 1, velocity meters were deployed as shown on Figure 4. Two MMB511's at 28.0 m from the right bank were mounted at vertical heights of 0.33 and 1.52 m above the river bottom. Three MMB511's at 43.0 m from the right bank were mounted at vertical heights of 0.36, 1.62, and 2.53 m above the riverbed. These meters were utilized to measure the variations of horizontal velocity components at various heights above the bed. The trip 1 wave gauge was 22.87 m from the right bank.

For trip 2, the velocity was measured at the locations shown in Figure 5. Three MMB511's at 41.1 m from the right bank were mounted at vertical heights of 0.51, 1.24, and 2.16 m above the riverbed. Two MMB511's at 68.6 m from the right bank were mounted at heights of 0.50 and 1.21 m above the bed. The trip 2 wave gauge was 18.3 m from the right bank.

Events

Discharges and stages were measured at different times during trip 1 and trip 2. Table 1 shows discharges, velocities, flow depths, and water surface elevations. The average water surface slope on this reach was 0.333 ft/mile (0.679 m/km) during trip 1 and 0.060 ft/mile (0.122 m/km) during trip 2. These slopes are determined by the daily stages at river mile 473.75 and river mile 468.2.

Trip 1 monitored 33 barge events and trip 2 monitored 28 barge events. Tables 2 and 3 (trips 1 and 2, respectively) give the name, date, draft, barge configuration, tow speed relative to earth, distance of the center line of the tow to the bank, and the tow direction for each event.

Data Filtering

Prototype and physical model data contain velocity and water level changes not caused by the tow. These changes included: the normal fluctuations found in turbulent flow, eddies shedding from upstream bends, and changes from upstream structures or tributaries. Model to prototype comparisons must be based on towinduced motion and not on extraneous components found in both the prototype and physical model. Filtering out unwanted information, if a limiting frequency can be identified, is one alternative. Since prototype tows are generally 300 m long and travel at about 3 m/sec, the time the tow is adjacent to the measuring point is about 100 sec, which roughly defines the period of the event and leads to a frequency of interest of 0.01 Hz. Data were filtered at a limiting frequency of 0.02 Hz to make certain that tow information is not filtered. Fluctuations above a certain frequency needed to be filtered out because model velocity, prototype velocity, and wave meters had different frequency response. For example, the prototype electromagnetic velocity meters sampled at 1 Hz, whereas the acoustic Doppler velocity meters used in the physical model sampled at 25 Hz, equivalent to 5 Hz in the prototype. A fast Fourier transform (FFT) filtered out components of velocity or drawdown occurring at frequencies greater than 0.02 Hz in both the

prototype and the physical model. Physical model data were filtered after scaling values to their prototype equivalent.

Tows Selected for Comparison to Physical Model

To achieve the first objective of the study, validation of the model, prototype events were selected to simulate in the physical model based on the following:

- *a.* Number of meters functioning during experiments. Some events were not used because one or more meters malfunctioned.
- b. Tow configuration and draft. To simulate tow events producing the maximum deviation from ambient conditions, only loaded barges that were three wide by four or five long were used in the adjustment/ calibration of the physical model. Events producing the maximum deviation from ambient were desired because small deviations from ambient conditions are difficult to extract from the ambient fluctuations found in the river. Also note that the 3-wide by 5-long, loaded tow is a standard configuration.

The eight tows initially selected were *JD Wofford*, *Pearl B.*, and *Donnie Ray Jr.*(2) from trip 1 and *Conti-Nan*(1), *Kevin Michael*, *Deborah Valentine*, *Kathy Ellen*, and *Cooperative Ambassador* from trip 2.

Definitions

Terms used herein are defined as follows:

- *a*. Left bank, or right of the thalweg, refers to a position in the cross section when looking at the cross section in a downstream direction.
- *b.* Ambient velocity is the velocity measured without tow traffic effects but close enough to the tow passage to eliminate variations due to flow and/or stage changes. At Clark s Ferry the prototype data presented for the *Kevin Michael* suggest that ambient velocity should be measured over at least 5 min to obtain a representation of the mean.
- *c.* Impact velocity is the maximum velocity or minimum velocity that occurs during the tow event for a given mechanism. For example, the impact velocity from return currents would be the maximum velocity (for upbound tows) or minimum velocity (for downbound tows) that occurs adjacent to the vessel. The return velocity is the difference between the impact velocity and the ambient velocity.

Ambient Velocity Fluctuations

The variation of the ambient velocity about the mean could establish the significance of tow-induced changes. For example, if natural stream velocity variations over periods of about 100 sec (100 sec based on duration of tow event) are ± 5 cm/sec, one might conclude that tow-induced changes less than 5 cm/sec are no different than the natural variations. The filtered prototype data were analyzed for the maximum and minimum values over a 100-sec time interval prior to any tow effects. The relative ambient velocity variation shown in Table 4 was found by dividing the difference between maximum and minimum values by two and then dividing by the mean ambient velocity. Using an average value from Table 4 as a guide, natural velocity fluctuations (with periods similar to a tow event period) fluctuate about the mean ambient current an average of ± 20 percent and ± 15 percent for the trip 1 and trip 2 data, respectively. The unfiltered prototype data for the eight verification tows were analyzed for standard deviation as a percentage of the mean ambient velocity at the velocity probe (referred to as the coefficient of variation, CV). CV values for trip 1 and trip 2 were 0.13 and 0.17, respectively. Whether using the maximum fluctuation over the duration of a tow event or the standard deviation, fluctuations in the river probably mask any towinduced return velocities that are less than about 15 percent of the mean ambient velocity.

Variation in Prototype Data

It is important to recognize that the prototype data in the verification process are subject to variation caused by measurement inaccuracy in tow speed, tow draft, tow position, tow alignment, water velocity, water level variation, and ambient discharge. Also of concern is the following: lack of knowledge about the propeller speed, applied horsepower, shape of the barge bow and the variation in the prototype cross sections up- and downstream of the cross section measured by the ISWS. All barges selected for the prototype verification had a 2.74-m draft. The writers' experience suggests that the loaded barges' draft could have been ± 0.15 m (6 in.). Tow alignment relative to the river axis could have been skewed by several degrees, resulting in an effective tow width greater than the sum of the barges' widths.

One of the greatest sources of uncertainty in the prototype data is extracting the tow impact from the ambient fluctuations in the river. This was not a problem for the trip 2 data, which were collected at low flow conditions. The relatively low return velocity (because of the large cross-sectional area) at Clark s Ferry in conjunction with the higher ambient velocities presents a problem for the trip 1 data. The changes induced by the tow in trip 1 are small and close to the magnitude of the natural velocity fluctuations having periods similar to the tow event. For example, the *JD Wofford* prototype data showed no significant change when the tow passed. The ambient velocity fluctuations from the filtered prototype data varied about an average of ± 18.5 percent of the mean velocity, which in absolute

terms was about ± 0.08 m/sec. The physical model data from *JD Wofford* showed that the average return velocity from the tow event was about 0.12 m/sec. The physical model value was difficult to determine because the physical model has variation about the mean of ± 0.06 m/sec. Since the tow change and the natural variations are close in magnitude for the trip 1 experiments, only the five tows from the trip 2 data will be used to calibrate the physical model.

To screen the prototype data for possible inconsistencies, the Schijf (1949) equation was used to compute the average return velocity and drawdown (Table 5). The Schijf equation provides a cross-sectional average return velocity whereas the prototype data are near bottom velocity data from which a maximum value was extracted. While these two velocities are different, their ratio should be relatively constant at a given meter, and meters physically close to each other should not vary significantly. Each tow event's prototype data were examined for a similar ratio of maximum observed return velocity/Schijf average return velocity. The filtered data from each prototype velocity meter were analyzed for the maximum return velocity/ Schijf average return velocity (Table 6). Velocity meters not close to the channel boundary would be expected to give similar values for a given tow event. Meters 999, 1000, 1131, 834, 151, 832, 642, 040, and 332 from trip 2 are not close to the boundary. One would also expect meters 999 and 1000 to give similar results because they are at the same lateral position and are located away from the channel perimeter. Meters 1131, 332, and 642 should also give the same response because of their similar positions. Based on Table 6, the only velocity meters in question are 151, 832, and 834 for the Deborah Valentine event because their values are less than the value from the Schijf equation whereas other events are greater. Meters 332 and 642 will not be used in the calibration/ verification because they are the same distance from the boundary and give the same result as meter 1131. Meter 1000 was omitted because it was at the same lateral position as 999 and because the physical model velocity meter at the position of 1000 malfunctioned for many of the experiments.

3 Physical Model Description

Similitude

Similarity of resistance, flow patterns, and water surface changes in navigation models is best achieved when the ratio of inertia to gravitational forces is the same in model and prototype. This ratio, the Froude number F, is defined as

$$F = \frac{V}{\sqrt{gD}} \tag{1}$$

where V is generally the vessel speed, g is the gravitational constant, and D is a characteristic length such as depth, draft, or vessel length. The equations of hydraulic similitude, based on the Froude criteria, expressed mathematical relations between the dimensions of hydraulic model and prototype quantities. General relations for transferring 1:30 scale model data to prototype equivalents are as follows:

Characteristic	Dimension ¹	Scale Relations Model: Prototype						
Length	Lr=Lp/Lm	1:30						
Area	A _r =L _r ²	1:900						
Velocity	$V_{r}=L_{r}^{1/2}$	1:5.48						
Time	$T_r = L_r^{1/2}$	1:5.48						
Discharge	$Q_r = L_r^{5/2}$	1:4929.5						
Roughness coefficient	$N_r = L_r^{1/6}$	1:1.76						
Force	Fr=Lr ³	1:27000						
Revolutions	$R_r = 1/L_r^{1/2}$	5.48:1						
¹ Dimensions are in terms of length.								

Viscous forces cannot be neglected in physical navigation models. If interest is in the forces on a vessel, the relatively higher viscous forces in the physical model cause greater frictional resistance on the model vessel. If the interest is in the forces the vessel imposes on the waterway (such as this study), the relatively higher viscous forces in the model cause the model vessel to be effectively larger than the prototype vessel. The following section on model calibration will show how this model dissimilarity is overcome.

Model Flume and Appurtenances

The navigation effects flume (Figures 6-8) is 125 m long, 21.3 m wide, and has a maximum 1.22-m depth. The last 1.52 m on both ends has a 2.13-m depth. Ten pumps, each having an approximate discharge capacity of 0.16 cu m/sec, recirculate flow through the flume. A sharp-crested overflow weir at the upstream end of the flume evenly distributes the flow across the flume.

The center 61 m of the flume was used for the 1:30-scale Clark's Ferry experimental reach. Marine plywood sections were installed to form the composite cross section representing 1.8 km of river conditions near mile 468.2 on the Mississippi River. The upstream end of the plywood section had curved entrance walls for a smooth transition into the experimental section. The data collected by the Mississippi River Hydrographic Survey in 1945 and in 1994 and data collected by the Illinois State Water Survey on 5/13/91 - 5/24/91 and 10/15/91 - 10/20/91 determined the composite cross section. This composite section was heavily weighted toward the ISWS data. The 1994 hydrographic survey was dike center-line elevations and some data on either side of the center line. One obvious difference between model and prototype was that the model was straight with a constant cross section. The coordinates of the section used in the physical model are shown as follows:

Distance from Thalweg, m	Design Elevation, NGVD	As-built at Sta 63 NVGD
-370.4 (top of left bank)	572.7	572.7
-370.4	538.0	548.0
-329.0	537.5	538.5
-256.1	537.4	538.2
-182.9	536.7	536.9
-73.2	530.7	531.1
0.0 (Thalweg)	528.8	528.8
109.8	530.0	531.0

Distance from Thalweg, m	Design Elevation, NGVD	As-built at Sta 63 NVGD
182.9	533.7	534.3
248.5	540.1	540.5
259.1	554.5	554.5
259.1 (top of right bank)	572.7	572.7

The same cross section was used along the full length of the 61-m-long plywood section. The left bank dikes shown in Figures 6 and 7 were about 340 m long, extended from the thalweg elevation of 528.8 up to el 538.0 at 85.3 m from the thalweg. From there the dikes extended over to el 539.0 at the left bank. The dikes were angled with the channel center line at 78 deg and the side slopes were 1V:3H.

The towboat (Figure 9) is modeled after the Corps' Motor Vessel Benyaurd and is 52 m long by 12.3 m wide by 2.74 m draft. The model towboat is equipped with two main and four flanking rudders, open-wheel, 2.74-m-diam propellers, and can be radio-controlled for self-propelled operation. The 1:30 scale plexiglass barges simulated 59.5 m long by 32 m wide by variable draft. Sets of barges were connected by C-clamps to form the desired tow configuration. All barges had boxed ends except for the lead barge, which had a raked end. Experiments were conducted with either a 45- or a 26-deg rake angle on the lead barge.

A towing carriage maintained consistent speed and alignment for the model tow and operated on steel rails set to grade that extended the length of the flume. The connection between the tow and the towing carriage was designed to allow complete freedom of vertical movement, push the tow at one point near the center of gravity, and maintain the desired tow alignment (Figure 10).

This study focuses on the far field effects of the tow. A previous study by Maynord (1990) conducted with and without propeller operation suggests the propeller has little impact on far field return velocity and drawdown adjacent to the vessel in these channel sizes. Analysis of the flow amount passing through the propellers shows that about 1 percent of the waterway is passing through the propellers, which suggests limited impact on far field effects. The Kampsville study (Maynord and Martin 1997) began with a series of experiments to further evaluate the effects of propeller flows on far field velocity and drawdown. Results of the physical model experiments suggested little impact but were not conclusive enough to conduct those experiments without propeller operation. Propeller operation was used in the Clark's Ferry experiments as well. Propeller speed had to be estimated, since prototype data collected by ISWS did not include the applied power or rpm. The model towboat was calibrated for bollard push (push when speed = 0) against propeller speed and applied voltage on a DC power supply. An equation developed by Toutant (1982) was used to define the bollard push (BP) for an open-wheel propeller as

$$BP_o = 23.57 (Hp)^{0.974}$$
(2)

or for a kort nozzle as

$$BP_k = 31.82(Hp)^{0.974} \tag{3}$$

where

BP = bollard push, pounds

hp = total horsepower

Knowing towboat horsepower from the ISWS data, the BP was computed using the Toutant equations. This BP provided an upper limit for a given horsepower towboat. The power setting, with some adjustment for tow speed, used 75 percent of the upper limit in most experiments.

Physical Model Instrumentation

The instrumentation was positioned laterally across the channel at approximately the midpoint of the plywood experimental section at station 63 (63 m from downstream end of concrete flume, Figure 6). A wave gauge and twodimensional (2-D) and three-dimensional (3-D) acoustic Doppler velocimeters (ADV's) are shown in Figure 11.

Wave heights were measured by using two wave gauges placed in the nearshore zone on both channel sides. The wave gauges were capacitance type gauges manufactured at the U.S. Army Engineer Waterways Experiment Station and sampled at 25 Hz.

Velocity measurements were taken using eight ADV's (Kraus, Lohrmann, and Cabrera 1994). Four probes were 3-D downward-looking probes and four were 2-D side-looking probes that measured velocity in the horizontal plane. One and sometimes two of the 3-D probes were upward-looking probes and the remainder were downward-looking probes. The ADV's took data approximately 5 cm from the transmit and receive transducers. The side-looking 2-D probes were needed for shallow-water velocities since the 3-D probes would not work in shallow water due to the 5-cm offset. The ADV's use acoustic sensing techniques to measure flow in a remote sampling volume. No cables were in the water and the measured flow is relatively undisturbed by the presence of the probe. Data were available at an output rate of up to 25 Hz. The horizontal velocity range is ± 2.5 m/sec and there is no zero-offset in the velocity output. Data can be collected as close as 5 mm from a solid boundary. The ADV's require that a certain size of particles be present in the water to measure the water velocity. Hollow glass spheres having a mean diameter of 10 microns and specific gravity slightly greater than

one were used as the seed material in the model. Under low or no ambient velocity conditions, a problem occurs with settlement of the seed between experiments. Generally, ambient velocities were high enough to keep seed in suspension. Positive x velocities were downstream and positive y velocities were toward the left bank.

Observations of ambient conditions in the physical model were found to have significant variations similar to the prototype. These variations were attributed to pump variations, eddies in the approach and exit to the plywood experimental section, and long-period oscillations in the basin set up by vessel movement. To overcome these variations, the physical model data were filtered like the prototype data. After scaling the physical model data to its prototype equivalent, an FFT filtered out all data with a frequency greater than 0.02 Hz.

4 Model Calibration

Introduction

In the model calibration, parameters in the physical model were adjusted until agreement was reached between the physical model and the ISWS prototype return velocity data from trip 2. The following four areas are suspected of causing differences between the model and prototype:

a. The physical model needs adjustment because the boundary layer along the vessel and along the channel perimeter grows faster in the physical model than in the prototype. This phenomenon occurs in all physical navigation models operated according to the previously presented Froudian scaling criteria. By equating the Froude number in a navigation model that is smaller than the prototype, the Reynolds number will be smaller in the model than in the prototype. The lesser Reynolds number in the model results in a faster growing boundary layer that causes the tow's effective size to be larger than the prototype. To quantify the boundary layer effects, the displacement thickness is computed, which indicates the distance by which the external streamlines are shifted owing to the formation of the boundary layer. Using the Prandtl-Schlichting skin friction equation for a smooth flat plate at zero incidence (Schlichting 1968) and computing the displacement thickness results in the following derived equation

$$\delta_1 = \frac{0.292L}{\left[Log\left(R_L\right)\right]^{2.58}} \tag{4}$$

where

- δ_1 = displacement thickness
- L = plate length, set equal to the total barge length herein
- R_L = plate Reynolds number defined as VL/v
- V = free stream velocity set equal to the vessel speed relative to the water and determined from $V = V_s + V_r + V_a$
- V_s = vessel speed relative to the ground
- V_r = average return velocity from Schijf

- V_a = ambient velocity (positive for upbound, negative for downbound)
- v = kinematic viscosity of water

In an unpublished study, a 1:37.5 scale navigation effects model was adjusted by reducing the draft of the barges to account for the dissimilarity of boundary layer. This comparison between model and prototype was approximate because the channel shape was a rough representation. Vessel length was 304.8 m. The required draft correction (D_c) is shown in Table 7. Model and prototype temperatures were 10 and 20 °C, respectively. In Table 7 all the dissimilarity between the boundary layer on the vessel and the channel perimeter have been lumped into conditions on the vessel. The draft correction can be computed from

$$D_C = C(\delta_{1m} - \delta_{1p}) \tag{5}$$

where *C* is the experimentally determined draft correction coefficient, δ_{1m} is the displacement thickness in the model scaled to its prototype equivalent, and δ_{1p} is the displacement thickness in the prototype. The effective draft becomes

$$d_e = d_a + D_C \tag{6}$$

where d_e is the effective draft and d_a is the actual draft. The Ohio and Illinois River results in Table 7 show *C* values of 1.18 and 1.68, respectively. The previous study on Kampsville on the Illinois River (Maynord and Martin 1997) resulted in an average *C* of 1.72 based on six tow events. These values will be compared to the required *C* for the Clark's Ferry experiments.

b. The second model/prototype source of scale effects results from flume length considerations. When starting the physical model from rest, flume length limitations dictate a faster acceleration than in the prototype. The acceleration for the physical model is shown in Figure 12. The tow in conjunction with the towing carriage becomes a wave generator that creates a wave in front of the tow. This wave is not as significant in the prototype because of the slower prototype acceleration and also tow motion is initiated much farther from the measurement point. The "wave-maker" in the prototype (the barges) generally is powered by about a 3,730-kW (5,000-hp) towboat whereas the towing carriage in the model has a scaled power of up to 112,000 kW (150,000 hp). Stated differently, the inertia of the vessel and the water in front of the vessel are significant compared to the power of the prototype tow and the resulting acceleration is low. The inertial forces in the model are small compared to the power of the carriage.

- *c*. The physical model flume length prohibits velocity/wave measurements for a significant time after tow passage because the startup wave generated by the tow bounces off the flume endwall and returns to the experimental section. Once this happens, the physical model data are not valid. Wave suppression devices are not effective for the long-period waves set up by vessel startup and are difficult to employ when flowing water is part of the experimental flume.
- *d.* The fourth area involves the unknown parameters from the prototype data such as the alignment (skew) of the tow, variations in the prototype cross section, and effects of the shape, particularly the bow, of the prototype barges. Uncertainties in both model and prototype measurements of speed, draft, tow position, etc., all contribute to differences between model and prototype.

The calibration process will show that the physical model reproduces the most significant tow displacement effects, the maximum return velocity. As stated earlier, the calibration will be based on the low-flow trip 2 tows because of the difficulty of extracting tow effects from the higher ambient velocities of trip 1. Since trip 2 prototype data did not have a recording wave gauge, calibration will be based on comparisons with return velocity only.

Verification

The Clark's Ferry verification process compared maximum return velocity for the tow events and developed rules for adjusting the model that resulted in agreement between model and prototype. All five tows from trip 2 were three barges wide, loaded to 2.74 m, and either four or five barges long. The ambient depthaveraged velocity distribution in the physical model for the trip 2 Pool 546.0 conditions is shown in Figure 13. For each of the prototype tows, five replicate runs of the physical model were conducted. At each probe, the five replicate runs were analyzed for maximum (or minimum) velocity alongside the tow, maximum drawdown, and the ambient velocity or water level before the tow effects arrived at the measurement location. These values were analyzed for outliers using the Chauvenet criterion given in Coleman and Steele (1989). This criterion specifies that all points should be retained that fall within a band around the mean that corresponds to a probability of 1-1/(2N) using Gaussian probabilities (where N is the number of experiments). For the five replicate experiments in Clark's Ferry, Chauvenet's criterion specifies that data were discarded only if they departed from the mean by more that $1.65S_x$ where S_x is the standard deviation of the sample of five points. All remaining experiments were averaged for comparison with the prototype data. The ambient velocities were averaged as were the maximum (or minimum) velocities alongside the tow for each probe. The difference between these two averages defined the maximum return velocity that represented the physical model for each probe.

The initial experiments were conducted with all physical model parameters scaled to the previously presented Froudian criteria, which requires geometric

similarity between model and prototype. Results comparing maximum return velocity for the Kevin Michael, Kathy Ellen, Deborah Valentine, Cooperative Ambassador, and Conti-Nan(1) are shown in Table 8. The physical model overestimates return velocity for most velocity meters when using geometric scaling and the Froude criteria. This was the expected result based on the boundary layer concerns presented above. The next series of experiments was conducted with reduced model barge draft to offset the greater boundary layer growth in the physical model. Also of concern at this stage was the startup wave, which was not present in the prototype data. Efforts were directed at reducing the magnitude of the startup wave because of concern that the presence of the startup wave might affect the return velocity and drawdown. Various model accelerations were tried with no significant impact, probably because the limited model length prevented significant reduction of the acceleration. The best agreement of return velocity was found with a 2.13-m draft on all barges. Results for the Kevin Michael, Kathy Ellen, and Deborah Valentine are presented in Tables 9, 10, and 11. This same draft correction was used to simulate the *Cooperative Ambassador* and *Conti-Nan(1)*. Results are shown in Tables 12 and 13.

Plots of prototype return velocity versus physical model return velocity are shown in Figures 14 and 15 for the 2.74- and 2.13-m drafts, respectively. Filtered time histories for the *Coop Ambassador* prototype and physical model data using the corrected draft are shown in Figures 16 to 25. Both prototype and model data demonstrate the difficulty in extracting changes caused by the tow from ambient fluctuations.

Draft Correction

In order to obtain an effective draft of 2.74 m, the actual draft is adjusted by the draft correction. The draft correction used for the five *Trip 2* calibration/ verification experiments was 2.74 m - 2.13 m = 0.61 m and is compared in Table 14 to the difference in displacement thickness for the tows used in the verification process. Omitting the *Kevin Michael*, which was the only four-bargelong tow, the verification experiments yield an average *C* for Equation 2 of 1.82, which is similar to the value determined in both previous experiments for the Illinois River (shown on Table 7 and in Maynord and Martin (1997)). A draft correction coefficient *C* of 1.72 will be used to compute D_C (Equation 5) and effective draft d_e (Equation 6) in the Clark's Ferry experiments.

These results show that the actual physical model draft along with the draft correction can be used to simulate the typical 2.74-m draft of loaded barges. However, the effective draft of an unloaded barge (about 0.6 m) cannot be obtained in the physical model. With a draft correction of approximately 0.61 m for five-barge-long tows, the minimum effective draft that can be obtained in the physical model is about 1.21 m at the 1:30 scale used herein.

5 Production Experiments and Analysis

Experiments evaluated the return velocity and drawdown for conditions and meter positions not addressed in the prototype experiments, after adjusting the physical model to reproduce the prototype. The verification experiments were conducted with the same lateral and vertical positions of the velocity and wave gauges in the model and prototype experiments. The vertical position of the velocity gauges in the production experiments was an issue that had to be resolved. Analysis of vertical velocity profile data (presented subsequently) shows that if the meter is too close to the bed, the maximum change resulting from tow passage may not be captured because the friction on the channel bottom retards the near-bottom velocities. The physical forces study also compared physical model results to a depth-averaged numerical model, HIVEL-2D (Stockstill, Martin, and Berger 1995). With the exception of the vertical velocity profile and the near dike experiments, all velocities in the production runs were measured at 60 percent of the local depth below the water surface. This position is standard for riverine surveys and ensured that the maximum change produced by the tow will be measured and could be directly compared to HIVEL-2D. The following paragraphs detail each experimental series.

Experimental Series 1—Pool Elevation 546.0

Experimental series 1 (pool 546.0), 5 (pool 551.5), and 7(pool 572.7) were used to evaluate the effects of a range of blockage ratios (channel area/vessel area) on the far-field effects of navigation. Twenty-four experiments (three replicates for each experiment) were conducted at a pool elevation of 546.0, with a discharge of 690 cms, using three-wide by five-long barges, and various tow speeds, directions, lateral positions, and drafts. The cross section is shown in Figure 26 and experimental conditions are summarized in Table 15. All experiments in this series were conducted with a 45-deg rake angle. Ambient velocity, maximum impact velocity, maximum return velocity, and drawdown below normal water level for each experiment are shown in Tables 16 to 39. To obtain a representative data set for the vector plots shown in Figures 27 to 50, the three replicate experiments were averaged and one was selected as the most representative of the mean of the three experiments. The vector plots are not based on one tow position with many different velocity meter positions as might be inferred from the vector plots. The vector plots were based on a single velocity meter position (Sta 63) and many different boat positions. Evaluating the vector plots is straightforward when the cross section is constant as in the case of the Kampsville study (Maynord and Martin 1997) where no dikes were present. When the cross section is variable, such as in the presence of the dikes at Clark's Ferry, the vector plots must be viewed with caution because the tow is a different distance from the dikes at each point in time. Because the vector plots can only provide a finite number of vectors, the maximum value was not always indicated but is provided in the tables. Table 40 summarizes the position of the velocity probes used in each experiment.

Experimental Series 2—Tow Length Experiments

Sixteen experiments (three replicates each) were conducted to determine the influence of the length of the barges on the navigation-induced forces. A pool elevation of 546.0 and a discharge of 690 cms was used with loaded barges, upbound and downbound, one sailing line, and variable boat speeds. Experimental conditions are summarized in Table 41. Ambient velocity, maximum impact velocity, maximum return velocity, and drawdown below normal water level for each experiment are shown in Tables 42 to 57. Vector plots for each representative experiment selected based on the mean of the three replicates are shown in Figures 51 to 66. Because the vector plots can only provide a finite number of vectors, the maximum value was not always indicated but is provided in the tables. Maximum return velocity for all four vessel speeds are plotted in Figures 67 and 68. Table 58 summarizes the position of the velocity probes used in each experiment. Plots of maximum drawdown versus vessel length for two speeds and left and right bank are shown in Figures 69 and 70. Both return velocity and drawdown in Figures 67 to 70 are normalized using the computed Schijf average return velocity or drawdown using the vessel speed relative to the water and the effective draft. The plots of return velocity show that the one- and two-barge-long tows tend to have high return velocity near the vessel and low return velocity away from the vessel compared to the longer vessels. Return velocity for the three-barge or longer tows are similar in magnitude. Drawdown, which was measured near the bank, was similar in magnitude for the four- and five-barge-long tows. Using vessel length to channel width as the pertinent ratio, results suggest that the return velocity and drawdown become constant for the four-barge-long vessels, which is L/B = 238/615 = 0.39. Additional work is being conducted with the numerical model HIVEL (Stockstill, Martin, and Berger 1975) to evaluate vessel length effects.

Experimental Series 3—Rake Experiments

Four experiments (three replicates each) were conducted to determine the influence of the rake configuration on the navigation-induced forces. The rake configuration refers to the shape of the bow of the lead barges. All experiments

conducted herein were conducted with boxed ends at all connections between barges. Previous experiments by Latorre and Ashcroft (1981) have shown a significant increase in the resistance of barges with increasing rake angle for a vessel Froude number (based on vessel length) of 0.1. At low vessel Froude numbers that are typical of UMRS tows (about 0.06), results from Latorre and Ashcroft show a small effect of tow configuration on barge resistance, but it is not known if this low Froude number effect also applies to rake angle. All previous 546.0 pool experiments were conducted with a 45-deg rake angle. Data were collected and evaluated for experiments run at variable speeds with a bow rake angle of 26 deg. A tow configuration of three wide by five long was used in these experiments. The 26-deg rake was created as a plexiglass extension to be added to the tow with the 45-deg rake. This increased the length of the tow by 7 m (28 cm in model). The experiments were conducted with a flow of 690 cms and a water surface elevation of 546.0. All experimental conditions were identical to the previous pool 546.0 experiments except for the rake angle. Experimental conditions are summarized in Table 59. Impact, ambient, and maximum return velocity and drawdown below normal water level for each experiment are shown in Tables 60 to 63. Vector plots for each representative experiment are shown in Figures 71 to 74. Because the vector plots can only provide a finite number of vectors, the maximum value was not always indicated but is provided in the tables. Plots of return velocity for the two rake angles and four vessel speeds are shown in Figures 75 and 76. The drawdown comparison for the 45-deg versus the 26-deg rake angle was inconclusive because of the scatter in the data. The difference between the return velocity caused by the 45-deg rake and the 26-deg rake is negligible. All experiments hereafter were done with a 26-deg rake.

Experimental Series 4—Vertical Velocity Distribution Experiments

Six experiments (three replicates each) were conducted to determine the vertical distribution of velocity changes induced by the tow. Experiments were conducted at a pool elevation of 546.0, with a discharge of 690 cms, three-wide by five-long barges, barges on thalweg, and loaded barges. Experimental conditions are shown in Table 64. Experiment LCVUCD (Table 65) shows the vertical distribution for an upbound tow and Experiment LCVDCD (Table 66) shows the vertical distribution for a downbound tow, 34 m left of the thalweg. Experiment LCVUBE (Table 67) shows the vertical distribution for an upbound tow and Experiment LCVDBE (Table 68) shows the vertical distribution for a downbound tow, 172 m left of the thalweg. Experiment LCVUAF (Table 69) shows the distribution for an upbound tow and Experiment LCVDAF (Table 70) shows the vertical distribution for a downbound tow, 318 m left of the thalweg. Results show a near uniform change in return velocity from 20 to 80 percent of the depth of flow from the bed. Results from Kampsville (Maynord and Martin 1997) show an upper zone where the return velocity is uniform and a lower zone where the near-bed velocity is retarded by the boundary resistance. The dividing line between the two zones was somewhere between 0.3 and 1.1 m above the bed for the depths used in the experiments.

Experimental Series 5—Pool Elevation 551.5

Twelve experiments (three replicates for each experiment) were conducted at a pool elevation of 551.5, with a discharge of 1,285 cms, a three-wide by fivelong barge configuration, and loaded barges. The cross section is shown in Figure 77 and experimental conditions are summarized in Table 71. Ambient, maximum impact velocity, maximum return velocity, and drawdown below normal water level for each test are shown in Tables 72 to 83. The ambient velocity distribution is shown in Figure 78. The three replicate tests were averaged and one of the three was selected as being most representative of the mean of the three tests. Vector plots for each representative test are shown in Figures 79 to 90. Because the vector plots can only provide a finite number of vectors, the maximum value was not always indicated but is provided in the tables. Table 84 summarizes the position of the velocity probes used in each test.

Experimental Series 6—Dike Experiments

Pool 551.5 dike experiments

Four experiments (three replicates each) were conducted at a pool elevation of 551.5, discharge of 1,285 cms, three-wide by five-long barge configuration, and loaded barges. All ADV's were moved from their normal position at the 63-m station downstream to the 59-m mark (keeping the lateral locations the same). Two probes were positioned directly on top of the dike and slightly upstream of 59 m. A plan view is shown in Figure 91. Experimental conditions are shown in Table 85. Impact, ambient and maximum return velocity, and drawdown below normal water level for each experiment are shown in Tables 86 to 89. Experiment H59D29 can be compared to HCD292, experiment H59D47 can be compared to HCD477, experiment H59U22 can be compared to HCU228, and experiment H59U41 can be compared to HCU416 as shown in Figure 92. Velocity for an upbound tow going 4.16 m/s is shown in Figures 93 and 94 for probes 3 and 4. Velocity for a downbound tow going 4.77 m/sec is shown in Figures 95 and 96 for probes 3 and 4. The dike velocities are greater for probe 3, which is the probe located on the part of the dike with the highest elevation. All other probes had a consistent velocity from the 63-m mark to the 59-m mark. Shapes of all velocities at the 59-m mark were consistent with those at the 63-m mark.

Pool 546.0 dike experiments

Detailed velocities were measured around the Clark's Ferry dike at the 70-m mark (first dike upstream of the 63-m location) and a generic dike having a different shape that was remolded at the 70-m mark. Both dikes had Clark's Ferry dikes upstream and downstream. Five velocity meters were placed around the base of the dike and one was positioned on the top of the dike. The instruments were placed 0.6 m off the bottom of the channel and off the top of the dike (Figure 97). All experiments were conducted with six dikes placed in the model

extending from the left bank to the thalweg at an angle of 78 deg upstream and spaced 304.7 m apart. The Clark's Ferry dike shape, referred to as the low dike, had a crest elevation of 539.0 on the left descending bank, to 538.0 at 85.3 m from the thalweg, to 528.8 on the thalweg. Each low dike was molded out of concrete and had a 3.0-m top width and a 1 on 3 slope down to the base at the channel bottom (see Figure 98). The generic dike shape, referred to as the high dike, had a constant crest elevation of 539.0, extending from the left bank to a point 4.7 m left of the thalweg. This elevation represents 60 percent of the total water depth at the thalweg. From this point the dike went down on a 1 on 1.5 slope to the channel bottom, elevation 528.8 (Figure 99). The high dike was formed by covering the low dike with riprap. All experiments were conducted with a pool elevation of 546.0 and a discharge of 690 cms, which resulted in an average channel velocity of 0.32 m/sec. Tow speeds relative to the ground during dike experiments were 3.82 m/sec for the downbound tow and 3.18 m/sec for the upbound tow, resulting in the same tow speed through the water for both tow directions. The tow had a three-wide by five-long barge configuration, an effective draft of 2.74 m, and a 26-deg rake on the lead barges. The sailing line was parallel to the ends of the dikes, 120 m right of the thalweg. During the experiment, velocities and direction of flow were determined for each probe location at various points in time. These points were determined by the position of the tow and its relationship to the dike. Data were recorded at eight points in time during each event. Each set of data was labeled with the position of the tow for both downbound (Figure100) and upbound runs (Figure 101). Velocities during tow passage are shown in Figures 102 to 105.

Experimental Series 7—Open River Experiment, Pool 572.7

Six experiments (three replicates of each) were conducted at a pool elevation of 572.7, with a three-wide by five-long barge configuration, and loaded barges. The open river tests required installation of vertical walls along the Clark's Ferry channel banks to simulate the larger open river depths. The Clark's Ferry water surface width is similar to the open river reach. A relatively low ambient velocity was used in the open river model tests to facilitate extraction of the tow effects, which were low because of the large section, from the ambient fluctuations. The cross section is shown in Figure 106 and experimental conditions are summarized in Table 90. Ambient, maximum impact velocity, maximum return velocity, and drawdown below normal water level for each experiment are shown in Tables 91 to 96. Velocity meters were positioned as in the Pool 551.5 experiments. Vector plots are shown in Figures 107 to 112.

Experimental Series 8—Drawdown Distribution

Detailed drawdown data were taken at six positions across the width of the channel. Results for Pool 546.0 with flow are shown in Tables 65 through 70. Drawdown data without flow were conducted at the higher pool elevations to

improve the extraction of the relatively low drawdown magnitude from the ambient fluctuations. Experimental conditions for pool elevation 551.5 are shown in Table 97. Results for pool 551.5 with no flow are shown in Tables 98 to 100. Experimental conditions for pool elevation 572.7 are shown in Table 101. Results for pool elevation 572.7 are shown in Tables 102 to 104.

6 Summary and Conclusions

Ambient flow conditions in both the Clark's Ferry physical model and the prototype had significant variations, which made extraction of the tow effects difficult. This was less of a problem in the previous Kampsville study (Maynord and Martin 1997) because the cross section was smaller, which caused the return velocity and drawdown to be larger. A fast Fourier transform filtered information above 0.02 Hz, but ambient fluctuations were present at the same frequency as the tow impact. Analysis of the Clark's Ferry prototype data show that the ambient fluctuations having about the same period as the tow impact average 15 percent of the mean ambient velocity.

Prototype return velocity was compared to physical model return velocity and showed that the Froude model with geometric scaling of vessel size resulted in model values greater than the prototype. The physical model draft had to be reduced from purely geometric scaling for agreement between model and prototype. The physical model also generated a wave and flow at the bow which was greater than the prototype data. This bow effect was likely related to the rapid acceleration that must be used in the physical model because of the limited flume length.

One of the primary purposes of this report was to provide data for a wide range of conditions. Return velocity and drawdown data were collected for several pool elevations, tow speeds, and upbound versus downbound vessels.

The vertical profile of return velocity was investigated to determine how to interpret and compare return velocities taken at different distances from the bottom. During passage of a tow, the flow depth can be separated into a lower zone in which the boundary layer growth can inhibit maximum return velocity and an upper zone in which the return velocity is nearly uniform. From the Kampsville study (Maynord and Martin 1997), the lower zone is generally confined to the lower 0.3 to 1.0 m of the depth and velocities are less in the lower zone. Measurements reported herein show a uniform velocity change at and above 20 percent of the depth from the bottom, which was the lowest position measured.

Tow length effects showed that the return velocity for tows one and two barges long (10 and 20 percent of the channel width) is high near the tow and low away from the vessel, compared to longer tows. Return velocity for tows three barges long (29 percent of channel width), is similar in magnitude to tows four or five barges long. Drawdown for tows four barges long (39 percent of channel width), is similar in magnitude to five-barge-long tows.

Return velocity and drawdown were compared for a vessel having a 26-deg and a 45-deg rake angle. Return velocity was similar for both angles. Scatter in the drawdown data for the two angles prevented a conclusion.

Velocity measurements near dikes were conducted for both upbound and downbound tows and show the change in velocity that occurs during tow passage.

Open river experiments were conducted by adding vertical walls along the banks of the Clark's Ferry channel to simulate the deeper depths found in the open river section. Return velocity and drawdown were measured with a low ambient velocity to allow extraction of the tow effect from ambient fluctuations. Use of typical open river ambient velocities would have made it difficult to extract return velocity and drawdown.

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Table 1Water Discharge, Average Velocity, Average Depth, and Water Surface Elevationfor the Clark's Ferry Site									
Date	ate Qw V D Water S cms m/s m Elevatio								
Trip 1									
05/14/91	2,351	0.83	4.41						
05/17/91				548.83					
05/19/91				549.35					
05/20/91				549.47					
05/21/91				549.61					
05/22/91	2,072	0.78	4.18	549.64					
05/23/91	2,428	0.85	4.36						
Trip 2									
10/17/91 - 10/20/91				546.0					
10/19/91	673	0.32	3.40	546.0					

Table 2 Traffic Characteristics, Trip 1													
Date	Vessel	Нр	Screws	Kort	Length m	Width m	Number of Barges	Config- uration	Barge Type	Draft m	Speed m/sec	Distance From Center Line to Bank m	Direction Bound
5/16	C. W. Rushing ₍₁₎	1,200	1	n	32.3	10.4	2	1x2	Cargo	2.74	2.02	325	Up
	Donnie Ray Jr (1)	5,600	2	у	53.7	12.2	15	3x5	Cargo	2.66	3.35	250	Down
	Samantha(1)	1,000	2	n	18.2	6.7	1	1x1	Coal	2.74	3.66	270	Down
	Samantha ₍₂₎	1,000	2	n	18.2	6.7	0			2.74	2.61	270	Up
5/17	Quad City Queen											250	Down
	C.W. Rushing ₍₂₎	1,200	1	n	32.3	10.4	1	1x1	Cargo	1.52	2.02	270	Down
	Jemco Towing						4	2x2	Cargo	2.74	2.97	275	Up
	T.S. Kunsman	4,200	2	n	45.7	10.7	12	3x4	Cargo	2.74	2.54	370	Down
	Dell Butcher	5,000	2	у	51.8	12.2	10	2x5	Cargo	2.74	2.16	270	Up
5/18	William Earthman	4,100	2	у	43.9	10.7	4	2x2	Chemical	1.52	2.54		Up
	Lady Lone Star	760	2	n	23.8	7.3	0			2.74	2.98	250	Up
5/19	Pearl B.	4,400	2	n	42.7	9.1	12	3x4	Cargo	2.74	2.87	250	Down
	Conti-Afton	4,200	2	n	42.7	13.4	15	3x5	Cargo	2.74	3.88	300	Down
	Jack D. Wofford	5,000	2	у	51.8	12.2	12	3x4	Cargo	2.74	3.70	300	Down
	Creole Belle	3,900	2	n	39.6	11.3	16	3x5+1	Empty	0.61	2.03	225	Up
5/20	Donnie Ray Jr ₍₂₎	5,600	2	у	53.7	12.2	15	3x5	Cargo	2.74	3.00	225	Up
	Sunflower	825	3	n	16.8	6.7	1	1x1	Cargo	0.61	5.59	250	Down
	America Beauty ₍₁₎	5,000	2	у	51.8	13.7	15	3x5	Cargo	0.61	3.23	275	Up
5/21	Sierra Dawn	5,000	2	у	50.0	12.2	12	3x4	Cargo	2.64	3.33	270	Down
	(Continued)												

Table 2 (Concluded)													
Date	Vessel	Нр	Screws	Kort	Length m	Width m	Number of Barges	Config- uration	Barge Type	Draft m	Speed m/sec	Distance from Center Line to Bank m	Direction Bound
	Cindy Erickson	3,900	2	n	36.6	11.6	15	3x5	Cargo	0.61	2.37	250	Up
	Frank H. Peavey	3,800	2	n	42.7	11.6	12	3x4	Cargo	2.74	3.28	275	Down
	Helen M. Clements	5,100	3	n	42.7	13.7	12	3x4	Cargo	0.61	2.51	260	Up
	Sunflowers (2)	825	3	n	16.8	6.7	1	1x1	Cargo	1.52	5.60	225	Down
	Dell Butcher(2)	5,000	2	у	51.8	12.2	12	3x4	Cargo	2.74	3.24	300	Down
	Hornet	4,300	2	n	44.5	11.6	12	3x4	Cargo	0.61	2.97	280	Up
	Volunteer State	4,320	2	n	45.7	14.6	15	3x5	Cargo	0.61	3.51	250	Up
	Enterprise Star						15	3x5	Cargo	2.74	3.51	275	Down
5/22	Edward J Hancock	4,320	2	у	45.1	10.4	13	3x4+1	Cargo	0.61	1.83	250	Up
	Joe/Nut	5,600	4	n	49.3	13.7	1			2.74	2.74	300	Up
	Starfire	3,200	2	n	47.6	10.7	10	1+3x3	Cargo	1.89	1.98	250	Up
	Conti-Karla	3,060	2	n	34.7	10.5	16	3x5+1	Cargo	0.74	2.00	275	Up
	America Beauty ₍₂₎	5,000	2	у	51.8	13.7	3	1+2x1	Cargo	1.52	5.18	300	Down
Table Traffic	3 c Characteristic	cs for T	rip 2										
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Date	Vessel	Нр	Screws	Kort	Length m	Width m	Number of Barges	Config- uration	Barge Type	Draft m	Speed m/sec	Distance from Center Line to Bank m	Direction Bound
10/17	C.W. Rushing	1,200	1	n	32.3	10.4	2	2x1	Hopper	1.52	3.98	220	Down
	Evey-T	4,300	2	n	42.7	11.6	13	1+3x4	Empty	0.61	2.41	260	Up
	Sunflower ₍₁₎	825	3	n	16.8	6.7	1	1x1	Empty	0.61	4.25	185	Down
	Evelyn C.	2,200	2	n	25.9	10.7	5	1+2x2	Corps work barge	2.74	1.92	220	Down
	Sunflower ₍₂₎	825	3	n	16.8	6.7	1	1x1	Hopper	2.74	3.13	210	Up
	Conti-Nan ₍₁₎	020		n			15	3x5	Hopper	2.74	2.41	260	Down
	Night 1			n			1	1x1	Work	2.74		250	Up
	Night 2			n			1	1x1	Hopper	1.52	4.25	230	Up
	Night 3			n			6	3x2	Work	2.74		230	Down
10/18	Lady Lone Star	760	2	n	23.8	7.3	1	1x1	Coal	2.74	2.38	200	Down
	Lady Lone Star	760	2	n	23.8	7.3	0			2.74	3.40	260	Up
	Kevin Michael	5,600	2	n	54.0	12.8	12	3x4	Closed hopper	2.74	2.31	245	Down
	Deborah Valentine	4,300	2	у	47.0	12.2	15	3x5	Closed hopper	2.74	2.14	210	Down
	Volunteer State	4,320	2	у	45.7	14.6	4	2x2	Closed hopper	2.74	4.25	185	Down
	Sunflower ₍₃₎	825	3	n	16.8	6.7	1	1x1	Closed hopper	0.61	4.25	230	Down
	Frank Stegbauer	3,200	2	n	39.6	10.7	3	1+2x1	Empty chemical	0.61	2.57	185	Down
													(Continued)

Table	3 (Concluded)												
Date	Vessel	Нр	Screws	Kort	Length m	Width m	Number of Barges	Config- uration	Barge Type	Draft m	Speed m/sec	Distance from Center Line to Bank m	Direction Bound
10/18	Joshua	1,000	2	n	18.3	6.7	1	1x1	Coal	2.74	2.48	240	Down
10/19	Kathy Ellen	3,800	2	n	46.0	10.7	15	3x5	Closed hopper	2.74	1.92	195	Down
	Jack Bullard	5,600	2	у	44.2	14.6	14	2x1+3x4	Hopper	2.74	2.38	215	Up
	Marc	1,000	2	n	18.3	6.7	4	2x2	Coal	2.74	2.70	205	Down
	Conti-Nan ₍₂₎	4,200	2	n	42.7	13.4	6	3x2	Empty chemical	0.61	2.84	185	Up
	Cristina Ecstein	3,200	2	n	35.4	10.5	8	3x2+2x1	Empty	0.61	2.88	215	Up
	Coast Guard 65504	600	2	n	19.8	6.4	1	1x1	Buoy tender/ work	2.74	4.95	225	Down
	Prairie Dawn	5,000	2	у	50.0	12.2	11	3x3+2	Empty	0.61	3.40	190	Up
10/20	Noname						2	2x1	Chemical	2.74	2.63	230	Down
	Coop Ambassador	3,800	2	у	48.8	12.2	15	3x5	Closed hopper	2.74	2.22	190	Down
	Yazoo City	4,300	2	n	44.8	10.7	14	2+3x4	Closed hopper		2.09	230	Up
	George W. Banta	2,400	2	n	30.2	9.1	3	1x3	Petroleum	2.74	2.00	200	Up

Table 4Relative Ambient Velocity Variation

						Meter						
Тоw	1001	1130	1131	998	999	1000	151	834	832	332	642	
			Trip 1	l (Avg. Ch	annel Velo	city 0.78 - 0).85 m/sec)				
JD Wofford	21	22	11	18	10	9	25	25	29	19	15	
	(0.22)	(0.41)	(0.51)	(0.40)	(0.62)	(0.68)	(0.24)	(0.39)	(0.30)	(0.52)	(0.51)	
Pearl B.	*	*	*	*	*	*	29	34	33	20	15	
	(*)	(*)	(*)	(*)	(*)	(*)	(0.15)	(0.25)	(0.21)	(0.50)	(0.51)	
Donnie Ray	26	18	14	23	14	13	*	*	*	23	17	
	(0.21)	(0.41)	(0.49)	(0.39)	(0.61)	(0.67)	(*)	(*)	(*)	(0.47)	(0.48)	
Avg. 24 20 13 21 12 11 29 30 31 21 16												
			Tr	ip 2 (Avg.	Channel V	elocity 0.32	2 m/sec)					
Conti-Nan	14	18	14	18	9	13	11	*	18	20	19	
	(0.12)	(0.25)	(0.28)	(0.18)	(0.23)	(0.25)	(0.33)	(*)	(0.30)	(0.26)	(0.25)	
K Michael	26	20	17	16	11	7	14	14	10	15	20	
	(0.09)	(0.22)	(0.25)	(0.16)	(0.22)	(0.24)	(0.30)	(0.41)	(0.27)	(0.23)	(0.23)	
Valentine	19	13	15	16	13	9	*	*	*	13	13	
	(0.10)	(0.23)	(0.26)	(0.12)	(0.21)	(0.23)	(*)	(*)	(*)	(0.23)	(0.23)	
K Ellen	24	14	11	18	10	11	13	14	16	19	17	
	(0.11)	(0.24)	(0.27)	(0.16)	(0.22)	(0.25)	(0.32)	(0.41)	(0.27)	(0.24)	(0.24)	
Ambassador	22	21	14	14	14	8	11	16	17	17	30	
	(0.11)	(0.24)	(0.27)	(0.19)	(0.22)	(0.24)	(0.31)	(0.39)	(0.28)	(0.23)	(0.25)	
Avg.	21	17	14	16	11	10	12	15	15	17	20	
Note: <u>(Maxir</u>	<u>num - Mini</u> (Am	mum)/(2 * bient at Ve	Ambient a elocity Prol	at Velocity be, m/sec)	Probe) * 10	0						

Table 5 Schijf Return Velocity and Drawdown for Trip 2 Verification Tows											
					Schijf						
Tow (Width x Length)	Direction Bound	Speed Through Water m/sec	Channel Area sq m	Channel Top Width m	Return Velocity m/sec	Drawdown m					
Conti-Nan (3x5)	Down	2.09	2,212	613	0.100	0.022					
K Michael (3x4)	Down	1.99	2,212	613	0.094	0.019					
Valentine (3x5)	Down	1.82	2,212	613	0.084	0.016					
K Ellen (3x5)	Down	1.60	2,212	613	0.072	0.012					
Ambassador (3x5)	Down	1.90	2,212	613	0.088	0.018					

Table 6 Maximum Retu	Table 6 Maximum Return Velocity/Schijf Average Return Velocity for Trip 2 Verification Tows											
					Meter							
Тоw	832	151	834	1131	999	1000	332	642	040			
Conti-Nan	1.47	1.39		1.50	1.40	1.26	1.47	1.68	*			
K Michael	1.42	1.22	1.28	1.36	1.13	1.22	1.31	1.10	*			
Valentine	0.65	0.49	0.73	1.30	1.22	1.11	1.31	1.35	*			
K Ellen	1.05	1.21	1.98	1.76	1.98	1.49	1.59	0.88	*			
Ambassador	1.08	1.43	1.55	1.27	1.22	1.09	1.10	1.18	*			

Table 7 Draft Corr	Table 7 Draft Correction (unpublished data)												
River	Vessel Speed m/sec	Return Velocity m/sec	DC m	δlm m	δlp m	δlm - δlp m	C = δlm - δlp						
Ohio	3.30	0.10	0.46	0.70	0.31	0.39	1.18						
Illinois	2.77	0.19	0.69	0.72	0.31	0.41	1.68						
δ _{lp} = Prototyp δ _{lm} = Model di	δ_{Ip} = Prototype displacement thickness δ_{Im} = Model displacement thickness * 37.5												

Table 8

Verification Data Using Geometrically Similar Froude Model, *Kevin Michael, Conti-Nan* (1), *Deborah Valentine, Kathy Ellen*, and *Coop Ambassador*

Probe Number	Physical Model, Return Velocity ¹ m/sec	Pototype Ambient Velocity, m/sec	Prototype Maximum Velocity, m/sec	Prototype Return Velocity ¹ m/sec
		Kevin Michael		
832	0.167	0.269	0.1356	0.1334
151	0.1806	0.301	0.1862	0.1148
834	0.0804	0.418	0.2977	0.1203
1131	0.1213	0.252	0.1238	0.1282
999	0.134	0.22	0.114	0.106
		Conti-Nan (1)		
832	0.1622	0.2980	0.1510	0.1470
151	0.1522	0.3280	0.1892	0.1388
834	0.0440			
1131	0.1343	0.2920	0.1420	0.1500
999	0.1460	0.2320	0.0920	0.1400
		Deborah Valentin	e	
832	0.1227	0.2670	0.2121	
151	0.1344	0.2980	0.2572	
834	0.0756	0.4170	0.3554	
1131	0.1596	0.2620	0.1526	0.1094
999	0.1527	0.2180	0.1158	0.1022
		Kathy Ellen		
832	0.0889	0.2730	0.1973	0.0757
151	0.1047	0.3190	0.2319	0.0871
834	0.1312	0.4080	0.2654	0.1426
1131	0.1341	0.2840	0.1573	0.1267
999	0.1254	0.2320	0.0892	0.1428
		Coop Ambassado	or	
832	0.1228	0.2940	0.1988	0.0952
151	0.1273	0.3010	0.1752	0.1258
834	0.0827	0.4080	0.2720	0.1360
1131	0.1562	0.2800	0.1679	0.1121
999	0.1831	0.2280	0.1204	0.1076
¹ Ambient - maxi	mum velocity.			

Table 9 Verificat	Table 9 Verification Data, Kevin Michael, Barge Draft 2.13 m													
		Physical N	Aodel Veloci	ity, m/sec, F	Replicate			Return Vel	ocity, m/sec ¹					
Probe Number	A	В	с	D	E	AVG	Prototype Velocity m/sec							
			Ambient	Velocity				Physical Model	Prototype					
832	0.2698	0.2780	0.2847	0.2957	0.2865	0.2829	0.269	0.1363	0.1334					
151 0.3072 0.2997 0.3054 0.3015 0.3091 0.3046 0.301 0.1409														
834	834 0.3034 0.3034 0.3033 0.3034													
1131	0.314	0.252	0.0817	0.1282										
999	0.3244	0.220	0.0939	0.1060										
			Minimum	Velocity										
832	0.1494	0.1465	0.1632	0.1475	0.1262	0.1466	0.1356							
151	0.1708	0.1650	0.1639	0.1642	0.1546	0.1637	0.1862							
834							0.297							
1131	0.2121	0.2333	0.2260	0.2419	0.2546	0.2336	0.1238							
999	0.2211	0.2254	0.2143	0.2348	0.2097	0.2211	0.1140							
			Physical	Model Drav	vdown, cm,	for Replica	ate							
	Α	В	с	D	E	AVG		Prototype I cm	Drawdown,					
	3.25	3.21	3.22	3.20	3.14	3.204								
¹ Ambient -	minimum vel	ocity.												

Table 10 Verificat	Table 10 Verification Data, Kathy Ellen, Barge Draft 2.13 m											
		Physical	Model Velo	city, m/sec,	Replicate			Return Vel	ocity, m/sec ¹			
Probe Number	А	В	с	D	E	AVG	Prototype Velocity m/sec	Dhusiaal				
			Ambien	t Velocity				Model	Prototype			
832	0.2789	0.2938	0.2761	0.2780	0.2730	0.2800	0.2730	0.0905	0.0757			
151	0.3093	0.2903	0.3047	0.2912	0.3059	0.3003	0.3190	0.1062	0.0871			
834	0.3784	0.3944	0.3801	0.3662	0.3773	0.3793	0.4080	0.1417	0.126			
1131	0.3186	0.3304	0.3160	0.3192	0.3159	0.3200	0.2840	0.1111	0.1267			
999	0.3222	0.1155	0.1428									
1000		0.2600		0.1072								
			Minimur	n Velocity								
832	0.1788	0.1905	0.1760	0.1975	0.2048	0.1895	0.1973					
151	0.1948	0.2097	0.1795	0.1819	0.2048	0.1941	0.2319					
834	0.2193	0.2494	0.2279	0.2413	0.2503	0.2376	0.2654					
1131	0.1918	0.2161	0.2012	0.2055	0.2300	0.2089	0.1573					
999	0.1831	0.2043	0.1992	0.2118	0.1958	0.1988	0.0892					
1000							0.1528					
			Physica	al Model Dra	wdown, cm	, for Replica	ate					
	А	в	с	D	E	AVG		Prototype I cm	Drawdown,			
	1.80	1.62	1.49	2.04	1.83	1.756		— ——				
¹ Ambient - /	minimum vel	locity.	<u>.</u>	<u>.</u>	<u>.</u>	<u>.</u>	<u>.</u>					

Table 11 Verificat	Table 11 Verification Data, Deborah Valentine, Barge Draft 2.13 m											
		Physical N	lodel Veloci	ity, m/sec, F	Replicate			Return Vel	ocity, m/sec ¹			
Probe Number	A	в	с	D	E	AVG	Prototype Velocity m/sec	Physical				
			Ambient	Velocity				Model	Prototype			
832	0.2972	0.2973	0.2857	0.2750	0.2646	0.2840	0.2670	0.1067				
151	0.2810	0.2895	0.2910	0.2886	0.3073	0.2915	0.2980	0.0985				
834	0.3620	0.3445	0.3568	0.3534	0.3540	0.3541	0.4170	0.1437				
1131	0.3514	0.3247	0.3378	0.3544	0.3458	0.3428	0.2620	0.1172	0.1094			
999	0.3217	0.2180	0.1128	0.1022								
	-		Minimum	Velocity	-							
832	0.1497	0.1941	0.1990	0.1596	0.1839	0.1773	0.2121					
151	0.1842	0.1903	0.2018	0.1994	0.1892	0.1930	0.2572	-				
834	0.1937	0.2163	0.2325	0.2030	0.2066	0.2104	0.3554	-				
1131	0.2315	0.2304	0.2212	0.2174	0.2273	0.2256	0.1526					
999	0.2153	0.1788	0.2114	0.1859	0.2124	0.2008	0.1158					
			Physical	Model Draw	/down, cm,	for Replica	ite					
	A B C D E AVG Prototype Drawdown, cm											
	2.64	2.68	2.32			2.547						
¹ Ambient -	Ambient - minimum velocity.											

Table 12 Verificat	Table 12 Verification Data, Coop Ambassador, Barge Draft 2.13 m											
		Physical I	Aodel Veloci	ity, m/sec, F	Replicate			Return Vel	ocity, m/sec ¹			
Probe Number	А	В	с	D	E	AVG	Prototype Velocity m/sec	Physical				
	-		Ambient	Velocity	-	-		Model	Prototype			
832	0.2887		0.2578	0.2675	0.2729	0.272	0.2940	0.0945	0.0952			
151	0.2788		0.3254	0.292	0.2994	0.299	0.3010	0.1123	0.1258			
834	0.3907	0.3652	0.3661	0.3746	0.361	0.372	0.4080	0.1449	0.1360			
1131	0.3072	0.3258	0.3126	0.3166	0.3025	0.313	0.2800	0.1232	0.1121			
999	0.3144	0.3246	0.3233	0.319	0.3258	0.321	0.2280	0.1319	0.1076			
			Minimum	Velocity								
832	0.1985		0.1722	0.1713	0.1666	0.1772	0.1988					
151	0.1881		0.1815	0.1948	0.1821	0.1866	0.1752					
834	0.2099	0.2592	0.1970	0.2205	0.2466	0.2266	0.2720					
1131	0.1941	0.1816	0.2038	0.1871	0.1820	0.1897	0.1679					
999	0.2101	0.1572	0.2059	0.2129	0.1612	0.1895	0.1204					
	·	·	Physical	Model Drav	vdown, cm,	for Replica	ate					
	Prototype Drawdown,											
	A	В	C	ט	E	AVG		cm				
	2.42 2.36 2.74 2.507											
¹ Ambient –	minimum ve	locity.										

Table 13 Verification Data, Conti-Nan (1), Barge Draft 2.13 m											
		Physical M	lodel Veloci	ity, m/sec, F	Replicate	Γ		Return Vel	ocity, m/sec ¹		
Probe Number	A	В	с	Prototype Velocity m/sec							
			Ar	mbient Velo	city			Physical Model	Prototype		
832	0.2623	0.2749	0.2716	0.2952	0.2669	0.2735	0.2980	0.1343	0.1470		
151	0.2834	0.3008	0.3154	0.3034	0.2914	0.2914	0.3280	0.1491	0.1388		
834	0.3601	0.3663	0.3553	0.3511	0.3541	0.3443		0.1331			
1131	0.3527	0.3385	0.3435	0.3465	0.342	0.3476	0.2920	0.1290	0.1500		
999	0.3237	0.3025	0.3281	0.3337	0.3194	0.3231	0.2320	0.1187	0.1400		
		-	Mi	nimum Velo	city	-					
832	0.1369	0.1443	0.1622	0.1208	0.1318	0.1392	0.1510				
151	0.1334	0.1341	0.1425	0.1824	0.1324	0.1450	0.1892				
834	0.2101	0.2132	0.2242	0.1963	0.2124	0.2112					
1131	0.2202	0.2069	0.2318	0.2316	0.2027	0.2186	0.1420				
999	0.2049	0.2038	0.1932	0.2207	0.1992	0.2044	0.0920				
		ite									
	A		Prototype I cm	Drawdown,							
	2.82	3.38	3.60	3.75	3.88	3.486					

¹ Ambient - minimum velocity.

Table 14 Draft Correction Computations							
		Temperature, °C		Kinematic Viscosity			
Tow	Length Prototype m	Model	Prototype	Model M**2/sec	Prototype 10**6		
K Michael	237.8	12.5	15	1.23	1.15		
Valentine	297.3	10.5	15	1.30	1.15		
K Ellen	297.3	9.0	9	1.36	1.36		
Conti-Nan (1)	297.3	14.0	11	1.18	1.28		
Ambassador	297.3	9.0	8.5	1.36	1.38		
Tow	Vessel Speed m/sec	Return Velocity m/sec	DC M	δlm m	δ <mark>lp</mark> m	δlm - δlp m	D _c C = δlm - δlp
K Michael	1.99	0.094	0.61	0.535	0.261	0.274	2.23
Valentine	1.82	0.084	0.61	0.662	0.320	0.342	1.79
K Ellen	1.60	0.072	0.61	0.678	0.333	0.345	1.77
Conti-Nan (1)	2.09	0.100	0.61	0.640	0.319	0.321	1.90
Ambassador	1.90	0.088	0.61	0.661	0.326	0.335	1.82
δ _{lp} = Prototype δ _{lm} = Model dis	displacement th	nickness. mess * 37.5.					

Experiment	Up			Table 15 Clark's Ferry Pool 546.0 Experiment Conditions							
No.	Or Down	Tow Speed ¹ m/sec	Position ²	Temp ° C	Actual Draft m	Effective Draft ³ m	Barge W X L	Prop Thrust 1,000 lb	Schijf Velocity⁴ cm/sec	Schijf Drawdown⁴ Cm	
LCU138	U	1.38	252.7	16	2.13	2.78	3X5	54	8.0	1.4	
LCU183	U	1.83	252.7	16	2.13	2.75	3X5	67.5	10.7	2.4	
LCU228	U	2.28	252.7	20.5	2.13	2.71	3X5	81	13.9	3.8	
LCU273	U	2.73	252.7	20.5	2.13	2.69	3X5	94.5	18.1	5.8	
LCU318	U	3.18	252.7	20.5	2.13	2.67	3X5	108	24.2	8.9	
									[
LCD202	D	2.02	252.7	18	2.13	2.77	3X5	54	8.0	1.4	
LCD247	D	2.47	252.7	16	2.13	2.75	3X5	67.5	10.7	2.4	
LCD292	D	2.92	252.7	16	2.13	2.72	3X5	81	13.9	3.8	
LCD337	D	3.37	252.7	16	2.13	2.70	3X5	94.5	18.1	5.8	
LCD382	D	3.82	252.7	16	2.13	2.68	3X5	108	24.2	9.0	
			-			-	-			-	
LRU228	U	2.28	131.7	20.5	2.13	2.71	3X5	81	13.9	3.8	
LRU318	U	3.18	131.7	20.5	2.13	2.67	3X5	108	24.2	8.9	
LRD292	D	2.92	131.7	16	2.13	2.72	3X5	81	13.9	3.8	
LRD382	D	3.82	131.7	16	2.13	2.68	3X5	108	24.3	9.0	
		1	1			1	1	-		1	
LLU228	U	2.28	294.7	18.5	2.13	2.71	3X5	81	13.9	3.8	
LLU318	U	3.18	294.7	18.5	2.13	2.67	3X5	108	24.2	8.9	
LLD292	D	2.92	294.7	16	2.13	2.72	3X5	81	13.9	3.8	
LLD382	D	3.82	294.7	16	2.13	2.68	3X5	108	24.3	9.0	
		1	1								
LCUU22	U	2.28	252.7	21.0	0.91	1.47	3X5	81	7.3	2.0	
LCUU31	U	3.18	252.7	21.0	0.91	1.44	3X5	108	12.3	4.5	
LCUU40	U	4.08	252.7	22.2	0.91	1.41	3X5	135	24.6	11.3	
	<u>ח</u>	2 92	252 7	22.2	0.91	1 47	385	81	73	2.0	
	<u>ס</u>	3.82	252.7	22.2	0.91	1 44	325	108	12.3	4.5	
	<u>р</u>	4.72	252.7	22.2	0.01	1.44	37.5 2 Y E	125	24.6	11.2	

Note: Water surface width 614.8 m, area 2170 sq m, q 690 cms, water surface elevation 546.0, average ambient velocity 0.32 m/sec, 45° rake. ¹ Relative to ground. ² Meters from right bank. ³ Actual draft + draft correction. ⁴ Schijf equation using effective draft and vessel speed relative to water.

Table 16 Clark's Feri	ry, Pool El 5	46.0, LCU138,	Run 17 Apr 9	95	
			Replicate		Return
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2492	0.2409	0.2417	0.2439	
2	0.2428	0.2404	0.2338	0.2390	
3	0.2923	0.2817	0.2809	0.2850	
4	0.3583	0.3584	0.3459	0.3542	
5	0.4293	0.4372	0.4176	0.4280	
6	0.4044	0.3866	0.4023	0.3978	
7	0.4011	0.4136	0.3944	0.4030	
8	0.1082	0.0963	0.1071	0.1039	
	·	Impact Velocity	, m/sec	·	
1	0.3212	0.3459	0.3577	0.3416	0.0977
2	0.3241	0.3495	0.3376	0.3371	0.0981
3	0.4147	0.4269	0.4340	0.4252	0.1402
4	0.5073	0.4977	0.5341	0.5130	0.1588
5	0.6136	0.5745	0.5763	0.5881	0.1601
6	0.5314	0.5174	0.5090	0.5193	0.1215
7	0.5595	0.5242	0.5403	0.5413	0.1383
8	0.1887	0.1554	0.1880	0.1774	0.0735
			Drawdown, cm		
Distance from Thalweg m		в	6	AVG	
196 m D	1.066	0.705		0.0205	
	1.000	0.795		0.9305	
1/1 m RB	1.378	0.795		1.0865	
¹ Impact - ambier	nt velocity.				

Table 17 Clark's Fer	ry, Pool El 5	46.0, LCU183,	Run 18 Apr §	95	
			Replicate		Return
Probe	А	в	с	AVG	Velocity ¹ m/sec
1	0.2412	0.2551	0.2412	0.2458	
2	0.2435	0.2416	0.2427	0.2426	
3	0.2954	0.2952	0.3157	0.3021	
4	0.3494	0.3638	0.3536	0.3556	
5	0.4506	0.4157	0.4096	0.4253	
6	0.4047	0.3887	0.3820	0.3918	
7	0.4198	0.3972	0.4064	0.4078	
8	0.1100	0.1040	0.0780	0.0973	
	I	Impact Velocity,	m/sec	I	
1	0.3217	0.3411	0.3179	0.3269	0.0811
2	0.3463	0.3395	0.3279	0.3379	0.0953
3	0.4233	0.4533	0.4419	0.4395	0.1374
4	0.5352	0.5515	0.5400	0.5422	0.1866
5	0.6312	0.6479	0.6217	0.6336	0.2083
6	0.5245	0.5483	0.5502	0.5410	0.1492
7	0.5469	0.5575	0.5658	0.5567	0.1489
8	0.1630	0.1754	0.1645	0.1676	0.0703
		ſ	Drawdown, cm		
Distance from Thalweg M	A	в	с	AVG	
186 m LB	1.3210	2.5190	2.3570	2.0660	
171 m RB	2.8570	6.3070	3.5900	4.2513	
¹ Impact - ambie	nt velocity.	1	1	l	

Table 18 Clark's Fer	ry, Pool El 5	546.0, LCU228,	Run 19 Apr 9	95	
			Replicate		Return
Probe	А	в	с	AVG	Velocity ¹ m/sec
1	0.2380	0.2387	0.2293	0.2353	
2	0.2345	0.2398	0.2238	0.2327	
3	0.2889	0.3007	0.2785	0.2894	
4	0.3598	0.3439	0.3393	0.3477	
5	0.3870	0.4126	0.3986	0.3994	
6	0.3740	0.3823	0.3931	0.3831	
7	0.4041	0.3950	0.3961	0.3984	
8	0.0945	0.1013	0.0986	0.0981	
	<u></u>	Impact Velocity	v, m/sec	I	
1	0.3586	0.3639	0.3949	0.3725	0.1372
2	0.3584	0.3619	0.3734	0.3646	0.1319
3	0.4798	0.4600	0.4797	0.4732	0.1838
4	0.6227	0.5788	0.5950	0.5988	0.2511
5	0.6726	0.6917	0.6706	0.6783	0.2789
6	0.5529	0.5731	0.5299	0.5520	0.1689
7	0.5935	0.5863	0.5383	0.5727	0.1743
8	0.2205	0.1995	0.1710	0.1970	0.0989
			Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	4.8720	5.3640	4.4000	4.8787	
171 m RB	5.5640	5.7450	5.2350	5.1470	
¹ Impact - ambie	nt velocity.				

Table 19 Clark's Ferr	ry, Pool El (546.0, LCU273	, Run 19 Apr §	95	
	<u> </u>		Replicate		Return
Probe	Α	В	с	AVG	Velocity ¹ m/sec
1	0.2334	0.2450	0.2427	0.2404	
2	0.2353	0.2282	0.2336	0.2323	
3	0.2904	0.2947	0.2779	0.2877	
4	0.3496	0.3475	0.3441	0.3471	
5	0.4098	0.3971	0.4122	0.4064	
6	0.3770	0.3838	0.3744	0.3784	
7	0.4036	0.3971	0.3893	0.3967	
8	0.0903	0.1137	0.0954	0.0998	
		Impact Velocity	y, m/sec	_	
1	0.4186	0.4175	0.4228	0.4196	0.1792
2	0.4313	0.4167	0.4152	0.4211	0.1888
3	0.5346	0.4983	0.4872	0.5067	0.2190
4	0.6262	0.6423	0.6470	0.6385	0.2914
5	0.7045	0.7038	0.7074	0.7052	0.2988
6	0.5665	0.5775	0.5882	0.5774	0.1990
7	0.6491	0.5919	0.6201	0.6204	0.2237
8	0.2151	0.2188	0.1993	0.2111	0.1113
			Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	5.3330	5.8330	6.4450	5.8703	
171 m RB	8.4450	7.7230	8.0000	8.0559	
¹ Impact - ambier	nt velocity.				

Table 20 Clark's Fer	ry, Pool El 5	546.0, LCU318,	Run 20 Apr 9	5	
			Replicate		Return
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2359	0.2415	0.2376	0.2383	
2	0.2412	0.2377	0.2407	0.2399	
3	0.2949	0.2888	0.2832	0.2890	
4	0.3441	0.3299	0.3526	0.3422	
5	0.4134	0.4304	0.3960	0.4133	
6	0.3854	0.3845	0.3851	0.3850	
7	0.3953	0.4081	0.3952	0.3995	
8	0.1132	0.1045	0.1061	0.1079	
		Impact Velocity	, m/sec		
1	0.5174	0.5314	0.4966	0.5151	0.2768
2	0.4794	0.4924	0.5055	0.4924	0.2525
3	0.5651	0.5699	0.5606	0.5652	0.2762
4	0.7298	0.7007	0.7160	0.7155	0.3733
5	0.7910	0.7431	0.7405	0.7582	0.3449
6	0.6497	0.6534	0.6096	0.6376	0.2526
7	0.6644	0.6300	0.6528	0.6491	0.2496
8	0.2818	0.2038	0.2440	0.2432	0.1353
			Drawdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	10.5560	9.8890	11.4450	10.6300	
171 m RB	9.9450	10.8890	9.2230	10.0189	
¹ Impact - ambie	nt velocity.				

Table 21 Clark's Ferr	ry, Pool El (546.0, LCD202	, Run 11 Apr 9	95	
			Replicate		Return
Probe	А	в	с	AVG	Velocity ¹ m/sec
1	0.2502	0.2505	0.2269	0.2425	
2	0.2354	0.2648	0.2316	0.2439	
3					
4	0.3425	0.3515	0.3345	0.3428	
5	0.4208	0.4087	0.3953	0.4083	
6	0.3750	0.3796	0.3761	0.3769	
7	0.3978	0.3707	0.3821	0.3835	
8		0.1165	0.0545	0.0855	
		Impact Velocity	y, m/sec		
1	0.1818	0.1802	0.1573	0.1731	0.0694
2	0.1849	0.1934	0.1678	0.1820	0.0619
3					
4	0.1863	0.2140	0.1583	0.1862	0.1566
5	0.2421	0.2366	0.2469	0.2419	0.1664
6	0.2845	0.2982	0.2526	0.2784	0.0985
7	0.2934	0.2678	0.2982	0.2865	0.0970
8		0.0659	0.0286	0.0473	0.0382
	·		Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	1.6670			1.6670	
171 m RB	1.9830			1.9830	
¹ Impact - ambie	nt velocity.				

Table 22 Clark's Feri	ry, Pool El {	546.0, LCD247	, Run 12 Apr 9	95	
			Replicate		Return
Probe	А	В	С	AVG	Velocity ¹ m/sec
1	0.2654	0.2481	0.2499	0.2545	
2	0.2463	0.2382	0.2484	0.2443	
3					
4	0.3678	0.3636	0.3520	0.3611	
5	0.4112	0.3987	0.3789	0.3963	
6	0.3707	0.3664	0.3566	0.3646	
7	0.3878	0.3865	0.3706	0.3816	
8	0.0517	0.1132	0.0982	0.0877	
		Impact Velocity	y, m/sec		
1	0.1267	0.1426	0.1489	0.1394	0.1151
2	0.1621	0.1478	0.1613	0.1571	0.0872
3					
4	0.1775	0.1674	0.1596	0.1682	0.1929
5	0.2680	0.2238	0.2452	0.2457	0.1506
6	0.2159	0.2469	0.2393	0.2340	0.1306
7	0.2878	0.2894	0.2517	0.2763	0.1053
8	0.0016	0.0413	0.0409	0.0279	0.0598
			Drawdown, cm		
Distance from Thalweg m	A	в	c	AVG	
186 m LB	2.9990	2.9530	2.6910	2.8810	
171 m RB	3.2000	3.5190	4.0770	3.5986	
¹ Impact - ambier	nt velocity.				

Table 23 Clark's Feri	ry, Pool El {	546.0, LCD292	, Run 13 Apr 9	95	
			Replicate		Return
Probe	А	в	С	AVG	Velocity ¹ m/sec
1	0.2171	0.2424	0.2252	0.2282	
2	0.2443	0.2423	0.2496	0.2454	
3	0.3052	0.2893	0.2888	0.2944	
4	0.3468	0.3378	0.3513	0.3453	
5	0.4147	0.4281	0.4183	0.4204	
6	0.3783	0.3929	0.3932	0.3881	
7	0.3889	0.3890	0.3983	0.3921	
8	0.1090	0.0897	0.0754	0.0914	
	l	Impact Velocity	y, m/sec		
1	0.1105	0.1148	0.1176	0.1143	0.1139
2	0.1094	0.1101	0.1245	0.1147	0.1307
3	0.1416	0.1377	0.1402	0.1398	0.1546
4	0.1261	0.1391	0.1331	0.1328	0.2125
5	0.1955	0.1620	0.1574	0.1716	0.2488
6	0.1972	0.2493	0.1932	0.2132	0.1749
7	0.2465	0.2709	0.2321	0.2498	0.1423
8	0.0066	0.0501	-0.0059	0.0169	0.0745
	• •		Drawdown, cm		
Distance from Thalweg m	A	в	c	AVG	
186 m LB	5.4000	5.4450	4.9630	5.2692	
171 m RB	4.8600	4.8890	4.9630	4.9038	
¹ Impact - ambier	nt velocity.				

Table 24 Clark's Feri	ry, Pool El 5	46.0, LCD337, I	Run 13 Apr 9	5	
		R	eplicate		Return
Probe	А	В	С	AVG	Velocity ¹ m/sec
1	0.2354	0.2276	0.2252	0.2294	
2	0.2355	0.2407	0.2464	0.2409	
3	0.2766	0.2872	0.2847	0.2828	
4	0.3450		0.3462	0.3456	
5	0.4233	0.4201	0.4297	0.4244	
6	0.3976	0.3844	0.3915	0.3912	
7	0.4075	0.4080	0.4077	0.4077	
8	0.0833	0.1206	0.0893	0.0977	
	1	Impact Velocity,	m/sec		
1	0.0735	0.0897	0.0759	0.7970	0.1497
2	0.0903	0.0687	0.0733	0.0774	0.1635
3	0.1123	0.0896	0.0929	0.0983	0.1845
4	0.1197		0.0867	0.1032	0.2424
5	0.1050	0.1385	0.0858	0.1098	0.3146
6	0.1978	0.1778	0.1954	0.1903	0.2009
7	0.2184	0.2063	0.1787	0.2011	0.2066
8	0.0050	-0.0185	0.0135	0.0000	0.0977
		D	rawdown, cm		
Distance from Thalweg m	А	В	с	AVG	
186 m LB	7.5900	7.1840	8.2710	7.6816	
171 m RB	7.1280	6.6840	6.9410	6.9177	
¹ Impact - ambier	nt velocity.				

Table 25 Clark's Fer	ry, Pool El {	546.0, LCD382,	Run 14 Apr 9	95	
			Replicate		Return
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2355	0.2626	0.2408	0.2463	
2	0.2288	0.2496	0.2550	0.2445	
3	0.2818	0.2871	0.2861	0.2850	
4	0.3712	0.3602	0.3550	0.3621	
5	0.4348	0.4196	0.4126	0.4223	
6	0.4063	0.4000	0.3889	0.3984	
7	0.4118	0.4130	0.4112	0.4120	
8	0.1154	0.1087	0.1266	0.1169	
	1	Impact Velocity	, m/sec	I	
1	-0.0287	0.0099	-0.0071	-0.0086	0.2549
2	0.0237	0.0095	0.0528	0.0287	0.2158
3	0.0539	0.0359	0.0314	0.0404	0.2446
4	0.0411	0.0353	-0.0125	0.0213	0.3408
5	0.0857	0.0812	0.0751	0.0807	0.3416
6	0.1474	0.1940	0.1519	0.1644	0.2340
7	0.1494	0.1145	0.1870	0.1503	0.2617
8	-0.0083	-0.0171	-0.0032	-0.0095	0.1264
			Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB					
171 m RB					
¹ Impact - ambie	nt velocity.				

Table 26 Clark's Feri	ry, Pool El s	546.0, LRU228	, Run 25 Apr 9	95	
	Replicate				
Probe	А	В	С	AVG	Velocity ¹ m/sec
		Ambient Veloci	ty, m/sec		
1	0.2784	0.2672	0.2611	0.2689	
2	0.2725	0.2641	0.2548	0.2638	
3	0.3335	0.3294	0.3175	0.3268	
4	0.4001	0.4181	0.3805	0.3996	
5	0.4149	0.4323	0.4209	0.4227	
6	0.4150	0.4152	0.4129	0.4144	
7	0.3742	0.3905	0.3738	0.3795	
8	0.0846	0.0945	0.0765	0.0852	
		Impact Velocity	y, m/sec		
1	0.3849	0.3552	0.3806	0.3736	0.1047
2	0.4001	0.3852	0.4001	0.3951	0.1313
3	0.4923	0.4695	0.4917	0.4845	0.1577
4	0.6111	0.5854	0.5551	0.5839	0.1843
5	0.7033	0.7289	0.6955	0.7092	0.2865
6	0.7755	0.7719	0.7604	0.7693	0.3549
7	0.6882	0.6817	0.7064	0.6921	0.3126
8	0.2937	0.2885	0.2484	0.2769	0.1917
	·		Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	4.1030	3.3740	3.4110	3.6292	
171 m RB	9.4360	9.5300	8.6410	9.2023	
¹ Impact - ambier	nt velocity.				

Table 27 Clark's Feri	y, Pool El 5	546.0, LRU318,	Run 25 Apr 9	5	
			Replicate		Return
Probe	А	в	с	AVG	Velocity ¹ m/sec
		Ambient Velocit	y, m/sec		
1	0.2605	0.2557	0.2603	0.2588	
2	0.2614	0.2731	0.2776	0.2707	
3	0.3233	0.3352	0.3374	0.3320	
4	0.3946	0.4142	0.4105	0.4064	
5	0.4042	0.4049	0.4149	0.4080	
6	0.4115	0.4080	0.4116	0.4104	
7	0.3722	0.3723	0.3688	0.3711	
8	0.0953	0.0821	0.1420	0.1065	
		Impact Velocity	v, m/sec		
1	0.5016	0.5061	0.5109	0.5062	0.2474
2	0.4826	0.4701	0.4913	0.4813	0.2106
3	0.5496	0.5828	0.5714	0.5679	0.2359
4	0.6540	0.6384	0.6573	0.6499	0.2435
5	0.8316	0.8241	0.8113	0.8223	0.4143
6	0.9380	0.9209	0.9177	0.9255	0.5151
7	0.8882	0.8666	0.8407	0.8652	0.4941
8	0.3356	0.3051	0.2811	0.3073	0.2008
	·		Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	8.3080	8.1200	7.7950	8.0743	
171 m RB	20.2940	19.8300	20.5890	20.1220	
¹ Impact - ambier	nt velocity.				

Table 28 Clark's Fer	ry, Pool El {	546.0, LRD292,	, Run 26 Apr 9	95	
		Return			
Probe	А	в	с	AVG	Velocity ¹ m/sec
		Ambient Velocit	y, m/sec		
1	0.2537	0.2572	0.2434	0.2514	
2	0.2455	0.2499	0.2706	0.2553	
3	0.3176	0.3146	0.3253	0.3192	
4	0.3954	0.3741	0.3848	0.3848	
5	0.3919	0.3934	0.3889	0.3914	
6	0.3893	0.3856	0.3763	0.3837	
7	0.3626	0.3554	0.3609	0.3596	
8	0.1043	0.0608	0.0760	0.0804	
	1	Impact Velocity	/, m/sec		
1	0.1528	0.1307	0.1457	0.1431	0.1084
2	0.1322	0.1256	0.1424	0.1334	0.1219
3	0.1733	0.1683	0.2227	0.1881	0.1311
4	0.2574	0.2692	0.2088	0.2451	0.1397
5	0.0999	0.1250	0.1649	0.1299	0.2615
6	0.1099	0.1201	0.0805	0.1035	0.2802
7	0.1245	0.1081	0.1202	0.1176	0.2420
8	-0.0509	-0.0907	-0.0957	-0.0791	0.1595
		·	Drawdown, cm	·	
Distance from Thalweg m	A	В	c	AVG	
186 m LB	2.4080	2.9240	2.4100	2.5807	
171 m RB	6.9070	8.3580	9.3330	8.1993	
¹ Impact - ambie	nt velocity.				

Table 29 Clark's Feri	ry, Pool El 5	546.0, LRD382,	Run 27 Apr 9	5	
	Replicate				
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2348	0.2502	0.2634	0.2495	
2	0.2466	0.2682	0.2492	0.2547	
3	0.3320	0.3297	0.3057	0.3225	
4	0.3686	0.3941	0.3662	0.3763	
5	0.3810	0.3846	0.3982	0.3879	
6	0.3857	0.3738	0.3746	0.3780	
7	0.3586	0.3542	0.3584	0.3571	
8	0.0770	0.0591	0.1064	0.0808	
		Impact Velocity	r, m/sec		
1	0.0755	0.0803	0.0718	0.0759	0.1736
2	0.0806	0.0962	0.0773	0.0847	0.1700
3	0.1318	0.1063	0.1554	0.1312	0.1913
4	0.2028	0.1755	0.1775	0.1853	0.1910
5	0.0574	0.0439	-0.0008	0.0335	0.3544
6	-0.0267	-0.0243	-0.0049	-0.0186	0.3966
7	-0.0155	-0.0152	0.0078	-0.0076	0.3647
8	-0.0827	-0.0463	-0.1277	-0.0856	0.1664
			Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	7.4440	7.9620	8.0280	7.8113	
171 m RB	10.0000	13.0550	13.4090	12.1547	
¹ Impact - ambier	nt velocity.				

Table 30 Clark's Feri	ry, Pool El :	546.0, LLU228,	Run 1 May 9	5	
	Replicate				
Probe	А	В	С	AVG	Velocity ¹ m/sec
1	0.2543	0.2553	0.2514	0.2537	
2	0.2441	0.2373	0.2447	0.2420	
3	0.3080	0.3118	0.3017	0.3072	
4	0.3106	0.3088	0.3221	0.3138	
5	0.3661	0.3477	0.3629	0.3589	
6	0.4076	0.4277	0.4180	0.4178	
7	0.4054	0.4195	0.4300	0.4183	
8	0.1077	0.1304	0.1353	0.1245	
		Impact Velocity	y, m/sec		
1	0.4345	0.4170	0.4156	0.4224	0.1687
2	0.3858	0.4151	0.3858	0.3956	0.1536
3	0.4958	0.5059	0.5115	0.5044	0.1972
4	0.6223	0.6128	0.6066	0.6139	0.3001
5	0.6183	0.6333	0.6154	0.6223	0.2634
6	0.6015	0.5649	0.6061	0.5908	0.1730
7	0.5924	0.5864	0.5741	0.5843	0.1660
8	0.1962	0.2198	0.2553	0.2238	0.0993
			Drawdown, cm		
Distance from Thalweg m	A	в	c	AVG	
186 m LB	6.2570	6.1020	6.2820	6.2137	
171 m RB	5.3840	5.2300	7.5380	6.0508	
¹ Impact - ambier	nt velocity.				

Table 31 Clark's Fer	ry, Pool El 5	646.0, LLU318,	Run 2 May 95	;	
			Replicate		Return
Probe	Α	В	с	AVG	Velocity ¹ m/sec
1	0.2679	0.2550	0.2580	0.2603	
2	0.2476	0.2376	0.2409	0.2420	
3	0.3072	0.3165	0.3074	0.3104	
4	0.3295	0.3330	0.3071	0.3232	
5	0.3775	0.3566	0.3499	0.3613	
6	0.3590	0.4123	0.4319	0.4011	
7	0.4236	0.4215	0.4095	0.4182	
8	0.1175	0.1499	0.1494	0.1389	
		Impact Velocity	, m/sec		
1	0.6409	0.6149	0.6389	0.6316	0.3713
2	0.5892	0.5828	0.5908	0.5876	0.3456
3	0.6963	0.6850	0.6553	0.6789	0.3685
4	0.7453	0.7361	0.7483	0.7432	0.4200
5	0.7481	0.7354	0.7419	0.7418	0.3805
6	0.7173	0.6897	0.7052	0.7041	0.2774
7	0.7047	0.6614	0.6899	0.6853	0.2671
8	0.2713	0.2884	0.2656	0.2751	0.1362
	·		Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	19.4440	17.8800	19.2310	18.8517	
171 m RB	9.8890	9.7700	9.8720	9.8437	
¹ Impact - ambier	nt velocity.				

Table 32 Clark's Fer	ry, Pool El 🤅	546.0, LLD292,	, Run 28 Apr 9	5	
			Replicate		Return
Probe	A	в	С	AVG	Velocity ¹ m/sec
		Ambient Veloci	ty, m/sec		
1	0.2460	0.2525	0.2529	0.2505	
2	0.2418	0.2496	0.2461	0.2458	
3	0.3208	0.3248	0.3043	0.3166	
4	0.3129	0.3282	0.3178	0.3196	
5	0.3416	0.3442	0.3727	0.3528	
6	0.4141	0.4116	0.4066	0.4108	
7	0.4175	0.3999	0.4179	0.4118	
8	0.1386	0.1249	0.1077	0.1237	
	1	Impact Velocity	y, m/sec	L	
1	0.1397	0.0535	0.0993	0.0975	0.1530
2	0.0740	0.0721	0.1164	0.0875	0.1583
3	0.1305	0.1317	0.1106	0.1243	0.1923
4	0.0892	0.0705	0.0797	0.0798	0.2398
5	0.1263	0.1714	0.1293	0.1423	0.2105
6	0.2204	0.2599	0.2292	0.2365	0.1743
7	0.2408	0.2334	0.2354	0.2365	0.1753
8	0.0443	0.0137	-0.0112	0.0156	0.1081
			Drawdown, cm	·	
Distance from Thalweg m	A	в	с	AVG	
186 m LB	7.5100	6.2050	5.6920	6.4690	
171 m RB	4.5330	4.6140	4.1540	4.4337	
¹ Impact - ambie	nt velocity.				

Table 33 Clark's Fer	ry, Pool El 5	546.0, LCD382,	Run 28 Apr 9	5	
			Replicate		Return
Probe	А	в	с	AVG	Velocity ¹ m/sec
		Ambient Velocit	y, m/sec		
1	0.2424	0.2506	0.2500	0.2477	
2	0.2348	0.2331	0.2283	0.2321	
3	0.2849	0.3076	0.3110	0.3012	
4	0.3060	0.3127	0.3044	0.3077	
5	0.3636	0.3520	0.3749	0.3635	
6	0.4162	0.4100	0.4044	0.4102	
7	0.4002	0.3858	0.3897	0.3919	
8	0.1041	0.0956	0.1001	0.0999	
	I	Impact Velocity	/, m/sec		
1	-0.0280	0.0039	-0.0291	-0.0177	0.2654
2	0.0027	-0.0434	-0.0825	-0.0411	0.2732
3	0.0457	0.0353	-0.0384	0.0142	0.2870
4	-0.0565	-0.0228	-0.0461	-0.0418	0.3495
5	0.0435	0.0581	0.0206	0.0407	0.3228
6	0.1969	0.2095	0.1625	0.1896	0.2206
7	0.2391	0.2084	0.1960	0.2145	0.1774
8	-0.0065	-0.0173	-0.0505	-0.0248	0.1247
			Drawdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	13.2200	8.2810	9.2780	10.2596	
171 m RB	8.3360	11.3310	10.5550	10.0739	
¹ Impact - ambie	nt velocity.				

Table 34 Clark's Feri	ry, Pool El s	546.0, LCUU22	, Run 23 May	95	
Replicate					Return
Probe	А	в	С	AVG	Velocity ¹ m/sec
		Ambient Veloci	ty, m/sec		
1	0.2399	0.2284	0.2330	0.2338	
2	0.2497	0.2455	0.2538	0.2497	
3	0.3005	0.2943	0.2866	0.2938	
4	0.3496	0.3626	0.3604	0.3575	
5	0.3893	0.3784	0.3771	0.3816	
6	0.4250	0.4052	0.4022	0.4108	
7	0.4097	0.3990	0.3998	0.4028	
8	0.0777	0.0990	0.0693	0.0820	
		Impact Velocity	y, m/sec	I	
1	0.3238	0.3019	0.3274	0.3177	0.0839
2	0.3300	0.3272	0.3283	0.3285	0.0788
3	0.4255	0.4007	0.4073	0.4112	0.1174
4	0.5910	0.5809	0.5623	0.5781	0.2206
5	0.5703	0.5693	0.5375	0.5590	0.1774
6	0.5350	0.5219	0.4804	0.5124	0.1016
7	0.5268	0.5061	0.5104	0.5144	0.1116
8	0.2193	0.2006	0.2190	0.2130	0.1310
	·		Drawdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	2.8210	2.7700	2.6410	2.7438	
171 m RB	1.9480	1.6920	1.6990	1.7797	
¹ Impact - ambier	nt velocity.				

Table 35 Clark's Ferr	ry, Pool El 🤅	546.0, LCUU31	, Run 23 May	95	
Replicate					Return
Probe	А	в	С	AVG	Velocity ¹ m/sec
		Ambient Veloci	ty, m/sec		
1	0.2382	0.2429	0.2353	0.2388	
2	0.2533	0.2472	0.2450	0.2485	
3	0.2991	0.2867	0.3009	0.2956	
4	0.3556	0.3451	0.3487	0.3498	
5	0.3698	0.3996	0.3827	0.3840	
6	0.4012	0.4057	0.4089	0.4053	
7	0.3933	0.3980	0.4122	0.4012	
8	0.1119	0.0951	0.1110	0.1060	
		Impact Velocity	y, m/sec		
1	0.3936	0.3951	0.3891	0.3926	0.1538
2	0.4121	0.4164	0.3822	0.4036	0.1551
3	0.4558	0.4613	0.4620	0.4597	0.1641
4	0.6135	0.6249	0.5867	0.6084	0.2586
5	0.5965	0.6055	0.5877	0.5966	0.2126
6	0.5498	0.5618	0.5200	0.5439	0.1386
7	0.5412	0.5438	0.5744	0.5531	0.1519
8	0.2678	0.2167	0.2104	0.2316	0.1256
	·		Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	7.4680	7.2670	6.7040	7.1463	
171 m RB	4.1330	4.1990	4.2940	4.2087	
¹ Impact - ambie	nt velocity.				

Table 36 Clark's Feri	ry, Pool El 5	46.0, LCUU40	, Run 24 May	95	
	Replicate				
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2337	0.2393	0.2264	0.2331	
2	0.2537	0.2446	0.2425	0.2469	
3	0.2915	0.2743	0.3085	0.2914	
4	0.3621	0.3639	0.3487	0.3582	
5	0.3966	0.3864	0.3929	0.3920	
6	0.4262	0.4255	0.4195	0.4237	
7	0.4253	0.3917	0.3959	0.4043	
8	0.0839	0.1150	0.1225	0.1071	
		Impact Velocity	, m/sec		
1	0.5601	0.5391	0.5451	0.5481	0.3150
2	0.5088	0.5029	0.4998	0.5038	0.2569
3	0.5430	0.5522	0.5203	0.5385	0.2437
4	0.6637	0.6922	0.7029	0.6863	0.3281
5	0.7318	0.7021	0.7094	0.7144	0.3224
6	0.6580	0.6474	0.6464	0.6506	0.2269
7	0.6621	0.6576	0.6489	0.6562	0.2519
8	0.2012	0.2181	0.2390	0.2194	0.1123
			Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	13.7180	13.7170	14.4440	13.9597	
171 m RB	9.2310	8.4860	9.0000	8.9057	
¹ Impact - ambier	nt velocity.				

Table 37 Clark's Ferr	ry, Pool El 🤅	546.0, LCUD29	, Run 25 May	95	
			Replicate		Return
Probe	А	В	С	AVG	Velocity ¹ m/sec
		Ambient Veloci	ty, m/sec		
1	0.2356	0.2404	0.2360	0.2373	
2	0.2534	0.2324	0.2433	0.2430	
3	0.2864	0.2920	0.2938	0.2907	
4	0.3739	0.3455	0.3560	0.3585	
5	0.4027	0.3893	0.3834	0.3918	
6	0.4130	0.4137	0.4124	0.4130	
7	0.4138	0.4137	0.4183	0.4153	
8	0.0789	0.1067	0.0707	0.0854	
		Impact Velocity	y, m/sec		
1	0.1525	0.1854	0.1737	0.1705	0.0668
2	0.1908	0.1658	0.1851	0.1806	0.0624
3	0.1888	0.2236	0.2021	0.2048	0.0859
4	0.2547	0.2570	0.2299	0.2472	0.1113
5	0.2136	0.1883	0.1781	0.1933	0.1985
6	0.3157	0.2764	0.2775	0.2899	0.1231
7	0.2776	0.3150	0.3062	0.2996	0.1157
8	-0.0028	0.0127	0.0026	0.0042	0.0812
			Drawdown, cm		
Distance from Thalweg m	A	в	c	AVG	
186 m LB	2.1770	2.0880	2.1690	2.1447	
171 m RB	2.4010	2.3560	2.4460	2.4010	
¹ Impact - ambie	nt velocity.				

Table 38 Clark's Ferry, Pool El 546.0, LCUD38, Run 25 May 95								
		Return						
Probe	А	В	с	AVG	Velocity ¹ m/sec			
1	0.2327	0.2404	0.2313	0.2348				
2	0.2460	0.2630	0.2410	0.2500				
3	0.2828	0.3100	0.3010	0.2979				
4	0.3535	0.3524	0.3537	0.3532				
5	0.3912	0.3778	0.3618	0.3769				
6	0.4302	0.3967	0.3858	0.4042				
7	0.4152	0.3928	0.4046	0.4042				
8	0.1291	0.0874	0.0670	0.0945				
1	0.1294	0.1563	0.1302	0.1386	0.0962			
2	0.1409	0.1323	0.1444	0.1392	0.1108			
3	0.1596	0.1903	0.1537	0.1679	0.1300			
4	0.2007	0.1915	0.2038	0.1987	0.1545			
5	0.1572	0.1686	0.1274	0.1511	0.2258			
6	0.2621	0.2543	0.2280	0.2481	0.1561			
7	0.2197	0.2603	0.2539	0.2446	0.1596			
8	-0.0084	-0.0246	-0.0054	-0.0128	0.1073			
Drawdown, cm								
Distance from Thalweg m	A	В	с	AVG				
186 m LB	5.4120	4.6310	5.6360	5.2263				
171 m RB	3.6470	3.0530	2.9090	3.2030				
¹ Impact - ambier	nt velocity.		·	-				

Table 39 Clark's Fer	ry, Pool El 5	646.0, LCUD47	, Run 26 May	95				
		Return						
Probe	A	В	с	AVG	Velocity ¹ m/sec			
1	0.2303	0.2528	0.2320	0.2384				
2	0.2484	0.2416	0.2511	0.2470				
3	0.2931	0.2801	0.2933	0.2888				
4	0.3726	0.3680	0.3668	0.3691				
5	0.3768	0.3689	0.3762	0.3740				
6	0.4229	0.4048	0.4089	0.4122				
7	0.4254	0.4208	0.4262	0.4241				
8	0.0938	0.0969	0.1046	0.0984				
1	0.0799	0.0718	0.0225	0.0581	0.1803			
2	0.1166	0.1170	0.1166	0.1167	0.1303			
3	0.1496	0.1349	0.1542	0.1462	0.1426			
4	0.1420	0.1401	0.1543	0.1455	0.2236			
5	0.0976	0.0782	0.1073	0.0944	0.2796			
6	0.1611	0.1479	0.1856	0.1649	0.2473			
7	0.1572	0.1375	0.1280	0.1409	0.2832			
8	-0.0220	-0.0034	-0.0396	-0.0217	0.1201			
Drawdown, cm								
Distance from Thalweg m	A	В	с	AVG				
186 m LB	6.2970	6.0190	6.5280	6.2813				
171 m RB	9.7220	8.9820	10.0930	9.5990				
¹ Impact - ambie	nt velocity.							
Table 40 Clark's Ferry,	ิโable 40 Clark's Ferry, Pool El 546.0, Experiments, Meter Positions							
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		Probe Number						
Probe Position ¹ Experiment No.	1	2	3	4	5	6	7	8
PP1 (LCU138, LCU183, LCU228, LCU273, LCU318, LCD202, LCD247, LCD292, LCD337, LCD382, LCUU22, LCUU22, LCUU31, LCUU40, LCUD29, LCUD38, LCUD40)	321.0 Left	228.0 Left	126.0 Left	30.0 Left	30.0 Right	99.0 Right	168.0 Right	237.0 Right
PP2 ^{**} (LRU228, LRU318, LRD292, LRD382)	321.0 Left	216.0 Left	114.0 Left	12.0 Left	90.0 Right	150.0 Right	195.0 Right	240.0 Right
PP3 ^{**} (LLU228, LLU318, LLD292, LLD382)	321.0 Left	237.0 Left	159.0 Left	75.0 Left	15.0 Left	69.0 Right	150.0 Right	237.0 Right
¹ Probe position, dis	tance in m	eters from tha	lweg, looking	downstream	ı.			

Table 41 Clark's Ferry Pool 546.0 Experiment Conditions, Tow Length Experiment										
Experiment No.	Up or Down	Tow Speed ¹ m/sec	Position ²	Temp ° C	Actual Draft m	Effective Draft ³ m	Barge W X L	Prop Thrust 1,000 lb	Schijf Velocity⁴ cm/sec	Schijf Drawdown⁴ cm
LC1U22	U	2.28	252.7	21.0	2.13	2.29	3X1	81	11.6	3.1
LC1U31	U	3.18	252.7	21.0	2.13	2.27	3X1	108	20.2	7.4
LC1D29	D	2.92	252.7	21.0	2.13	2.29	3X1	81	11.6	3.1
LC1D38	D	3.82	252.7	21.0	2.13	2.27	3X1	108	20.2	7.4
				-	-		-	_		
LC2U22	U	2.28	252.7	21.0	2.13	2.41	3X2	81	12.2	3.3
LC2U31	U	3.18	252.7	21.0	2.13	2.39	3X2	108	21.4	7.9
LC2D29	D	2.92	252.7	21.0	2.13	2.41	3X2	81	12.2	3.3
LC2D38	D	3.82	252.7	21.0	2.13	2.39	3X2	108	21.4	7.9
LC3U22	U	2.28	252.7	21.0	2.13	2.51	3X3	81	12.8	3.5
LC3U31	U	3.18	252.7	21.0	2.13	2.49	3X3	108	22.4	8.2
LC3D29	D	2.92	252.7	21.0	2.13	2.51	3X3	81	12.8	3.5
LC3D38	D	3.82	252.7	21.0	2.13	2.47	3X3	108	22.2	8.2
LC4U22	U	2.28	252.7	18.5	2.13	2.61	3X4	81	13.3	3.6
LC4U31	U	3.18	252.7	18.5	2.13	2.57	3X4	108	23.2	8.5
LC4D29	D	2.92	252.7	18.5	2.13	2.61	3X4	81	13.3	3.6
LC4D38	D	3.82	252.7	18.5	2.13	2.58	3X4	108	23.2	8.5

Note: Water surface width 614.8 m, area 2170 sq m, q 690 cms, water surface elevation 546.0, average ambient velocity 0.32 m/sec, 45° rake. ¹ Relative to ground. ² Meters from right bank. ³ Actual draft + draft correction. ⁴ Schijf equation using effective draft and vessel speed relative to water.

Table 42 Clarks Ferr	y, Pool El 5	46.0, LC1U22,	Run 19 May 9	95	
			Replicate		Return
Probe	А	В	С	AVG	Velocity ¹ m/sec
1	0.2542	0.2373	0.2461	0.2459	
2	0.2546	0.2544	0.2607	0.2566	
3	0.2987	0.3050	0.3085	0.3041	
4	0.3773	0.3723	0.3491	0.3662	
5	0.3653	0.3753	0.3969	0.3792	
6	0.3986	0.4131	0.4109	0.4075	
7	0.3976	0.4136	0.4161	0.4091	
8	0.0943	0.1226	0.0942	0.1037	
		Impact Velocity	y, m/sec		
1	0.3143	0.2932	0.4077	0.3384	0.0925
2	0.3296	0.3291	0.4210	0.3599	0.1033
3	0.4229	0.4285	0.4948	0.4487	0.1446
4	0.7391	0.2757	0.8081	0.6076	0.2414
5	0.7042	0.7113	0.8083	0.7413	0.3621
6	0.5165	0.5159	0.5886	0.5403	0.1328
7	0.4677	0.5059	0.5726	0.5154	0.1063
8	0.1677	0.1955	0.2121	0.1918	0.0881
			Drawdown, cm		
Distance from Thalweg m	A	в	c	AVG	
186 m LB		3.3760	3.5760	3.4760	
171 m RB	1.5900	2.0900	2.0000	1.8933	
¹ Impact - ambier	nt velocity.				

		F	Replicate		Return
Probe	А	в	с	AVG	m/sec
		Ambient Velocity	, m/sec		
1	0.2308	0.2461	0.2456	0.2408	
2	0.2450	2,607.0000	0.2569	0.2542	
3	0.2938	0.3085	0.2864	0.2962	
4	0.3578	0.3491	0.3501	0.3523	
5	0.3931	0.3969	0.3993	0.3964	
6	0.3878	0.5592	0.4070	0.4513	
7	0.4088	0.5037	0.4129	0.4418	
8	0.1040	0.0942	0.1011	0.0998	
	·	Impact Velocity,	m/sec		
1	0.4325	0.3063	0.4248	0.3879	0.1471
2	0.4141	0.3166	0.4131	0.3813	0.1271
3	0.5257	0.4184	0.5261	0.4901	0.1939
4	0.8466	0.7271	0.8319	0.8019	0.4496
5	0.8081	0.6883	0.8158	0.7707	0.3743
6	0.5957	0.5592	0.5933	0.5827	0.1314
7	0.5921	0.5037	0.6068	0.5675	0.1257
8	0.1724	0.2473	0.2051	0.2083	0.1085
		D	rawdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	9.3220	9.2470	8.3770	8.9820	
171 m RB	6.9440	6.9450	6.5670	6.8187	

Table 44 Clark s Feri	y, Pool El	546.0, LC1D29,	Run 18 May	95	
			Replicate		Return
Probe	A	В	с	AVG	Velocity ¹ m/sec
1		0.2401	0.2542	0.2472	
2		0.2700	0.2507	0.2604	
3		0.2872	0.3175	0.3024	
4		0.3541	0.3803	0.3672	
5		0.3833	0.3826	0.3830	
6		0.4981	0.4060	0.4521	
7		0.4094	0.4077	0.4086	
8		0.0970	0.0962	0.0966	
	•	Impact Velocity	, m/sec	I	
1		0.1908	0.1965	0.1937	0.0535
2		0.1963	0.1881	0.1922	0.0682
3		0.2146	0.2225	0.2186	0.0838
4		0.0462	0.0864	0.0663	0.3009
5		0.0931	0.0424	0.0678	0.3152
6		0.2909	0.3077	0.2993	0.1528
7		0.2954	0.3278	0.3116	0.0970
8		-0.0001	-0.0032	-0.0017	0.0983
	·		Drawdown, cm		
Distance from Thalweg m	A	в	c	AVG	
186 m LB		1.5660	2.8200	2.1930	
171 m RB		1.6330	1.4870	1.5600	
¹ Impact - ambie	nt velocity.		•		· · · · · · · · · · · · · · · · · · ·

Table 45 Clark's Fer	ry, Pool El (546.0, LC1D38,	Run 18 May	95	
			Replicate		Return
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2371	0.2396	0.2384	0.2384	
2	0.2532	0.2440	0.2478	0.2483	
3	0.2965	0.3080	0.3040	0.3028	
4	0.3788	0.3795	0.3653	0.3745	
5	0.4008	0.3838	0.4038	0.3961	
6	0.4441	0.4173	0.4163	0.4259	
7	0.4252	0.4127	0.4171	0.4183	
8	0.1006	0.1068	0.0892	0.0989	
	1	Impact Velocity	, m/sec	I	
1	0.1292	0.0775	0.1267	0.1111	0.1273
2	0.1117	0.1301	0.1424	0.1281	0.1202
3	0.1523	0.1017	0.1323	0.1288	0.1740
4	-0.0196	-0.0103	0.0021	-0.0093	0.3838
5	0.0122	0.0247	0.0264	0.0211	0.3750
6	0.2458	0.2375	0.2390	0.2408	0.1851
7	0.3143	0.3267	0.2830	0.3080	0.1103
8	0.0084	0.0314	0.0048	0.0149	0.0840
			Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	8.4290	7.9310	6.9650	7.7750	
171 m RB	1.9990	1.7250	1.5810	1.7473	
¹ Impact - ambie	nt velocity.				

Table 46 Clark's Feri	ry, Pool El s	546.0, LC2U22	, Run 12 May	95	
			Replicate		Return
Probe	А	В	С	AVG	Velocity ¹ m/sec
1	0.2357	0.2353	0.2234	0.2315	
2	0.2464	0.2427	0.2500	0.2464	
3	0.2975	0.2927	0.3042	0.2981	
4	0.3641	0.3712	0.3717	0.3690	
5	0.3784	0.3989	0.3823	0.3865	
6	0.4160	0.4237	0.4204	0.4200	
7	0.4100	0.4091	0.4113	0.4101	
8	0.1105	0.1131	0.1099	0.1112	
	1	Impact Velocity	y, m/sec		
1	0.3228	0.3177	0.3410	0.3272	0.0957
2	0.3716	0.3616	0.3417	0.3583	0.1119
3	0.4452	0.4134	0.4459	0.4348	0.1367
4	0.6188	0.5864	0.6139	0.6064	0.2374
5	0.6334	0.6405	0.6249	0.6329	0.2464
6	0.5644	0.5492	0.5094	0.5410	0.1210
7	0.5282	0.5279	0.5084	0.5215	0.1114
8	0.1881	0.2249	0.1859	0.1996	0.0884
	·		Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	3.2460	2.3200	3.6450	3.0703	
171 m RB	2.6210	2.4600	2.8870	2.6560	
¹ Impact - ambier	nt velocity.				

Table 47 Clark's Feri	ry, Pool El 🤅	546.0, LC2U31	, Run 12 May	95	
			Replicate		Return
Probe	А	В	С	AVG	Velocity ¹ m/sec
1	0.2377	0.2222	0.2408	0.2336	
2	0.2443	0.2649	0.2506	0.2533	
3	0.3002	0.3040	0.2962	0.3001	
4	0.3608	0.3747	0.3527	0.3627	
5	0.3667	0.3964	0.3901	0.3844	
6	0.4002	0.4085	0.4189	0.4092	
7	0.4018	0.4059	0.4089	0.4055	
8	0.1059	0.1024	0.1026	0.1036	
	1	Impact Velocity	y, m/sec	I	
1	0.4551	0.3835	0.3713	0.4033	0.1697
2	0.4609	0.4320	0.3970	0.4300	0.1767
3	0.5428	0.5047	0.5214	0.5230	0.2229
4	0.8108	0.7164	0.7411	0.7561	0.3934
5	0.8171	0.7230	0.7420	0.7607	0.3763
6	0.6567	0.6420	0.5979	0.6322	0.2230
7	0.6152	0.6047	0.5803	0.6001	0.1946
8	0.2249	0.2057	0.2239	0.2182	0.1146
			Drawdown, cm	·	
Distance from Thalweg m	A	в	с	AVG	
186 m LB	9.5370	6.8660	6.2430	7.5487	
171 m RB	5.6020	5.1340	4.8480	5.1947	
¹ Impact - ambier	nt velocity.	·			

Table 48 Clark's Feri	ry, Pool El (546.0, LC1U22	, Run 19 May 9	95	
			Replicate		Return
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2353	0.2358	0.2425	0.2379	
2	0.2483	0.2437	0.2535	0.2485	
3	0.2956	0.2916	0.2988	0.2953	
4	0.3496	0.3554	0.3560	0.3537	
5	0.3972	0.3948	0.3809	0.3910	
6	0.4158	0.4295	0.4090	0.4181	
7	0.4157	0.4101	0.4112	0.4123	
8	0.1019	0.1019	0.1052	0.1030	
		Impact Velocity	y, m/sec		
1	0.1705	0.1804	0.1764	0.1758	0.0621
2	0.1779	0.1607	0.1577	0.1654	0.0831
3	0.1486	0.1813	0.1925	0.1741	0.1212
4	0.0900	0.1454	0.2136	0.1497	0.2040
5	0.1205	0.1262	0.1371	0.1279	0.2631
6	0.2031	0.2320	0.2457	0.2269	0.1912
7	0.2739	0.3004	0.2959	0.2901	0.1222
8	0.0315	0.0150	-0.0442	0.0008	0.1022
	·		Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	1.9640	2.9830	2.1000	2.3490	
171 m RB	4.1070	2.6170	3.3330	3.3523	
¹ Impact - ambier	nt velocity.				

Table 49 Clark's Fer	ry, Pool El 54	46.0, LC2D38,	Run 15 May	95	
			Replicate		Return
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2269	0.2391	0.2277	0.2312	
2	0.2466	0.2380	0.2442	0.2429	
3	0.2991	0.2914	0.2756	0.2887	
4	0.3572	0.3518	0.3530	0.3540	
5	0.3746	0.3993	0.3888	0.3876	
6	0.4077	0.4138	0.4214	0.4143	
7	0.4057	0.4072	0.3663	0.3931	
8	0.0906	0.0926	0.1039	0.0957	
	1	Impact Velocity	, m/sec		
1	0.0669	0.0473	0.0665	0.0602	0.1710
2	0.1106	0.0966	0.1191	0.1088	0.1341
3	0.0718	0.1219	0.0911	0.0949	0.1938
4	0.0008	0.1132	0.1225	0.0788	0.2752
5	0.0270	0.0278	0.0155	0.0234	0.3642
6	0.1642	0.1934	0.1601	0.1726	0.2417
7	0.2691	0.2534	0.2820	0.2682	0.1249
8	-0.0208	-0.0652	-0.0366	-0.0409	0.1366
	·		Drawdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	8.3780	7.7780		8.0780	
171 m RB	4.3780	4.8150		4.5963	
¹ Impact - ambie	nt velocity.				

Table 50 Clark's Fer	ry, Pool El (546.0, LC3U22	, Run 10 May	95	
			Replicate		Return
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2375	0.2518	0.2424	0.2436	
2	0.2554	0.2482	0.2394	0.2477	
3	0.2994	0.3019	0.2907	0.2973	
4	0.3728	0.3634	0.3578	0.3647	
5	0.3721	0.3883	0.4118	0.3907	
6	0.4115	0.4173	0.4172	0.4153	
7	0.3838	0.4067	0.4239	0.4048	
8	0.1129	0.1056	0.1179	0.1121	
	1	Impact Velocity	y, m/sec		
1	0.3465	0.3331	0.3469	0.3422	0.0986
2	0.3658	0.3529	0.3545	0.3577	0.1100
3	0.4676	0.4750	0.4677	0.4701	0.1728
4	0.6207	0.6188	0.6151	0.6182	0.2535
5	0.6100	0.6377	0.6097	0.6191	0.2284
6	0.5495	0.5859	0.5569	0.5641	0.1488
7	0.5484	0.5614	0.5201	0.5433	0.1385
8	0.1876	0.1950	0.3094	0.2307	0.1186
			Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	4.0000	3.1180	2.7540	3.2907	
171 m RB	2.1550	2.2590	2.4680	2.2938	
¹ Impact - ambie	nt velocity.				

Table 51 Clark's Fer	ry, Pool El 🤅	546.0, LC3U31	, Run 9 May 9	5	
			Replicate		Return
Probe	Α	В	С	AVG	welocity ⁻ m/sec
1	0.2346	0.2329	0.2329	0.2335	
2	0.2481	0.2476	0.2428	0.2462	
3	0.3004	0.2880	0.2801	0.2895	
4	0.3491	0.3628	0.3509	0.3543	
5	0.3896	0.3860	0.3872	0.3876	
6	0.3994	0.4060	0.4017	0.4024	
7	0.4100	0.4055	0.4151	0.4102	
8	0.0845	0.0880	0.1057	0.0927	
	<u></u>	Impact Velocity	y, m/sec	<u>l</u>	
1	0.4702	0.4587	0.4900	0.4730	0.2395
2	0.4636	0.4691	0.4707	0.4678	0.2216
3	0.5698	0.5553	0.5585	0.5612	0.2717
4	0.7038	0.6885	0.5009	0.6311	0.2768
5	0.6918	0.6741	0.6993	0.6884	0.3008
6	0.6235	0.6329	0.6481	0.6348	0.2324
7	0.6148	0.6307	0.5968	0.6141	0.2039
8	0.2431	0.2254	0.1880	0.2188	0.1261
			Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	9.4340	9.6230	9.3400	9.4657	
171 m RB	5.4700	6.1320	6.1320	5.9113	
¹ Impact - ambie	nt velocity.				

Table 52 Clark's Fer	ry, Pool El (546.0, LC3D29	, Run 8 May 9	5	
			Replicate		Return
Probe	А	В	С	AVG	Velocity ¹ m/sec
1	0.2323	0.2435	0.2263	0.2340	
2	0.2600	0.2439	0.2348	0.2462	
3	0.3038	0.3016	0.2855	0.2970	
4	0.3550	0.3593	0.3654	0.3599	
5	0.3816	0.4005	0.3746	0.3856	
6	0.3935	0.4289	0.4079	0.4101	
7	0.4036	0.4027	0.4088	0.4050	
8	0.1154	0.0609	0.0988	0.0917	
	1	Impact Velocity	y, m/sec		
1	0.1512	0.1608	0.1238	0.1453	0.0887
2	0.1510	0.1736	0.1370	0.1539	0.0923
3	0.1948	0.1701	0.1594	0.1748	0.1222
4	0.1354	0.1318	0.1161	0.1278	0.2321
5	0.1377	0.1383	0.1473	0.1411	0.2445
6	0.2626	0.2600	0.2630	0.2619	0.1482
7	0.2184	0.2194	0.2977	0.2452	0.1598
8	0.0369	0.0087	0.0019	0.0158	0.0759
			Drawdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	3.1340	1.8420	2.1070	2.3610	
171 m RB	2.8670	3.2370	3.6420	3.2487	
¹ Impact - ambie	nt velocity.				

Table 53 Clark's Ferr	ry, Pool El 5	546.0, LC3D38,	, Run 9 May 9	5	
			Replicate		Return
Probe	Α	В	С	AVG	Velocity ¹ m/sec
1		0.2363	0.2379	0.2371	
2		0.2441	0.2429	0.2435	
3		0.2957	0.2956	0.2957	
4		0.3432	0.3455	0.3444	
5	0.3711	0.3626	0.3840	0.3726	
6	0.4019	0.4167	0.3990	0.4059	
7	0.4171	0.4267	0.3956	0.4131	
8	0.0741	0.0855	0.0943	0.0846	
		Impact Velocity	/, m/sec		
1		0.0404	0.0366	0.0385	0.1986
2		0.0597	0.0731	0.0664	0.1771
3		0.0605	0.0633	0.0619	0.2338
4		0.0533	0.0263	0.0398	0.3046
5	0.0665	0.0639	0.0847	0.0717	0.3009
6	0.2197	0.1697	0.1343	0.1746	0.2313
7	0.2271	0.2462	0.1907	0.2213	0.1918
8	-0.0572	-0.0054	0.0114	-0.0171	0.1017
	<u> </u>		Drawdown, cm	<u> </u>	<u> </u>
Distance from Thalweg m	A	В	c	AVG	
186 m LB	10.9430	9.2450	9.1510	9.7797	
171 m RB	5.3770	5.4700	6.3200	5.7223	
¹ Impact - ambie	nt velocity.				

Table 54 Clark's Fer	ry, Pool El	546.0, LC4U22	, Run 4 May 9	5	
	Replicate			Return	
Probe	А	В	С	AVG	Velocity' m/sec
		Ambient Veloci	ty, m/sec		
1	0.2535	0.2224	0.2334	0.2364	
2	0.2475	0.2381	0.2479	0.2445	
3	0.2836	0.2887	0.2824	0.2849	
4	0.3514	0.3490	0.3637	0.3547	
5	0.3639	0.3769	0.3850	0.3753	
6	0.4279	0.4029	0.3995	0.4101	
7	0.4277	0.3990	0.4091	0.4119	
8	0.0395	0.0817	0.1118	0.0777	
	1	Impact Velocity	y, m/sec	1	
1	0.3663	0.3551	0.3397	0.3537	0.1173
2	0.3800	0.3765	0.3818	0.3794	0.1349
3	0.4593	0.4868	0.4501	0.4654	0.1805
4	0.5798	0.6002	0.6017	0.5939	0.2392
5	0.6146	0.6023	0.5879	0.6016	0.2263
6	0.5959	0.5736	0.5567	0.5754	0.1653
7	0.5540	0.5746	0.5570	0.5619	0.1500
8	0.1716	0.1974	0.2042	0.1911	0.1134
			Drawdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	4.4880	4.0880	4.4880	4.3547	
171 m RB	4.8890	4.5310	5.1080	4.8427	
¹ Impact - ambie	nt velocity.				

Table 55 Clark's Fer	ry, Pool El 5	546.0, LC4U31,	Run 4 May 9	5	
			Replicate		Return
Probe	А	В	с	AVG	Velocity ¹ m/sec
1	0.2406	0.2259	0.2270	0.2312	
2	0.2516	0.2421	0.2462	0.2466	
3	0.2969	0.2837	0.3074	0.2960	
4	0.3443	0.3465	0.3595	0.3501	
5	0.3816	0.3775	0.3543	0.3711	
6	0.4064	0.4039	0.3951	0.4018	
7	0.4142	0.3982	0.4088	0.4071	
8	0.0842	0.1002	0.0903	0.0916	
	1	Impact Velocity	, m/sec		
1	0.4632	0.4793	0.4804	0.4743	0.2431
2	0.5016	0.4986	0.4951	0.4984	0.2518
3	0.5702	0.5767	0.5804	0.5758	0.2798
4	0.6650	0.6849	0.7279	0.6926	0.3425
5	0.6923	0.6946	0.7238	0.7036	0.3325
6	0.6370	0.6346	0.6707	0.6474	0.2456
7	0.6267	0.6523	0.6604	0.6465	0.2394
8	0.2037	0.2332	0.2131	0.2167	0.1251
			Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	11.2150	11.0000	11.6660	11.2937	
171 m RB	8.4600	8.8880	9.1100	8.8193	
¹ Impact - ambie	nt velocity.				

Table 56 Clark's Fer	ry, Pool El {	546.0, LC4D29	, Run 5 May 9	5	
			Replicate		Return
Probe	Α	В	c	AVG	Velocity ¹ m/sec
1	0.2337	0.2272	0.2431	0.2347	
2	0.2478	0.2529	0.2467	0.2491	
3	0.2953	0.2880	0.2904	0.2912	
4	0.3533	0.3385	0.3521	0.3480	
5	0.3721	0.3841	0.3751	0.3771	
6	0.4023	0.4094	0.3968	0.4028	
7	0.4131	0.4057	0.4032	0.4073	
8	0.0996	0.0693	0.0890	0.0860	
		Impact Velocity	y, m/sec	I	
1	0.1229	0.1332	0.1645	0.1402	0.0945
2	0.1278	0.1388	0.1442	0.1369	0.1122
3	0.1413	0.1430	0.1754	0.1532	0.1380
4	0.1583	0.1157	0.1287	0.1342	0.2138
5	0.1347	0.1065	0.1266	0.1226	0.2545
6	0.2401	0.2285	0.2348	0.2345	0.1683
7	0.2753	0.2726	0.2219	0.2506	0.1567
8	-0.0065	0.0100	-0.0153	-0.0039	0.0899
			Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	4.8160	4.5250	4.1070	4.4827	
171 m RB	4.9870	4.8420	4.9990	4.9427	
¹ Impact - ambie	nt velocity.				

Table 57 Clark's Feri	ry, Pool El 54	6.0, LC4D38, R	un 5 May 95		
		Re	plicate		Return
Probe	A	в	С	AVG	Velocity ¹ m/sec
1	0.2311	0.2331	0.2408	0.2350	
2	0.2321	0.2463	0.2400	0.2395	
3	0.2481	0.2836	0.2775	0.2817	
4	0.3410	0.3423	0.3560	0.3464	
5	0.3675	0.3722	0.3876	0.3758	
6	0.4032	0.3845	0.3981	0.3953	
7	0.3914	0.3921	0.3918	0.3918	
8	0.1301	0.0839	0.0670	0.0937	
		Impact Velocity, m	/sec		
1	0.0659	-0.0115	0.0387	0.0310	0.2040
2	0.0187	0.0588	0.0308	0.0361	0.2034
3	0.0455	0.0525	0.0826	0.0602	0.2215
4	0.0624	0.0837	0.1064	0.0842	0.2622
5	0.0895	0.0747	0.0469	0.0704	0.3054
6	0.2022	0.0863	0.1552	0.1479	0.2474
7	0.2122	0.1850	0.1514	0.1829	0.2089
8	0.0054	0.0050	-0.0494	-0.0130	0.1067
		Dra	awdown, cm	<u> </u>	<u></u>
Distance from Thalweg m	A	в	c	AVG	
186 m LB	11.1110	11.4820	11.2710	11.2880	
171 m RB	6.7600	6.7600	6.9800	6.8333	
¹ Impact - ambier	nt velocity.		•	<u> </u>	

Table 58 Clark's Ferry, Pool El 546.0, Tow Length Experiments, Meter Positions

	Probe Number							
Probe Position ¹ Experiment o.	1	2	3	4	5	6	7	8
PP1 (LC1U22, LC1U31, LC1D29, LC1D29, LC1D38, LC2U22, LC2U31, LC2D38, LC2U29, LC2D38, LC3U22, LC3U31, LC3D29, LC3D38, LC4U22, LC4U31, LC4D29, LC4D38)	321.0 Left	228.0 Left	126.0 Left	30.0 Left	30.0 Right	99.0 Right	168.0 Right	237.0 Right

Clark's Ferry Pool 546.0 Experiment Conditions – Rake Experiments Up Tow Or Speed ¹ Temp Draft Draft ³ Barge Thrust Velocity ⁴ Schijf Drawdown ⁴										
No.	Down	m/sec	Position ²	°℃	m	m	WXL	1,000 lb	cm/sec	cm
LCEU22	U	2.28	252.7	24.0	2.13	2.68	3X5	81	13.7	3.7
LCEU31	U	3.18	252.7	24.0	2.13	2.64	3X5	108	23.9	8.8
LCED29	D	2.92	252.7	22.5	2.13	2.68	3X5	81	13.7	3.7
LCED38	D	3.82	252.7	24.0	2.13	2.65	3X5	108	24.0	8.9
Note: Water: 0.32 m/sec, 2 ¹ Relative to g ² Meters from ³ Actual draft	surface w 6° rake. round. right ban + draft co	ridth 614.8 k. rrection.	m, area 2,170	sq m, q 69	90 cms, wa	ater surface e	elevation 54	46.0, averaç	je ambient v	elocity

⁴ Schijf equation using effective draft and vessel speed relative to water.

Table 60 Clark's Feri	ry, Pool El 54	6.0, LCEU22, R	un 6 Jun 95		
		Re	plicate		Return
Probe	А	В	с	AVG	Velocity' m/sec
1	0.2395	0.2262	0.2326	0.2328	
2	0.2498	0.2468	0.2571	0.2512	
3	0.2957	0.2970	0.2962	0.2963	
4	0.3627	0.3545	0.3507	0.3560	
5	0.3740	0.3917	0.3817	0.3825	
6	0.4077	0.4104	0.4064	0.4082	
7	0.3922	0.4031	0.4038	0.3997	
8	0.0790	0.1212	0.0825	0.0942	
		Impact Velocity, m	/sec		
1	0.3653	0.3782	0.3689	0.3708	0.1380
2	0.3907	0.3963	0.4090	0.3987	0.1475
3	0.4956	0.4826	0.4923	0.4902	0.1939
4	0.6158	0.6783	0.6472	0.6371	0.2811
5	0.6335	0.6702	0.6269	0.6435	0.2610
6	0.5779	0.5394	0.5705	0.5626	0.1544
7	0.5769	0.5667	0.5631	0.5689	0.1692
8	0.1731	0.2396	0.2205	0.2111	0.1169
		Dra	wdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	4.7550	5.3850	6.0010	5.3803	
171 m RB	5.9530	5.0260	5.6410	5.5401	
¹ Impact - ambier	nt velocity.				

Table 61 Clark's Feri	ry, Pool El 546	6.0, LCEU31, R	un 6 Jun 95		
		Rep	olicate		Return
Probe	А	В	с	AVG	Velocity' m/sec
1	0.2197	0.2462	0.2273	0.2311	
2	0.2452	0.2489	0.2417	0.2453	
3	0.2865	0.2983	0.2990	0.2946	
4	0.3530	0.3556	0.3692	0.3593	
5	0.3865	0.3856	0.3660	0.3794	
6	0.4072	0.4035	0.3919	0.4009	
7	0.3949	0.3930	0.4133	0.4004	
8	0.0840	0.0803	0.0915	0.0853	
		Impact Velocity, m/	/sec		
1	0.5533	0.5267	0.5492	0.5431	0.3120
2	0.5536	0.5311	0.5300	0.5382	0.2929
3	0.6291	0.6179	0.6424	0.6298	0.3352
4	0.7440	0.7480	0.7586	0.7502	0.3909
5	0.7333	0.7175	0.7202	0.7237	0.3443
6	0.6700	0.6788	0.6539	0.6676	0.2667
7	0.6621	0.6571	0.6751	0.6648	0.2644
8	0.2705	0.1799	0.2096	0.2200	0.1347
		Dra	wdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	13.6660	14.1110	14.3330	14.0367	
171 m RB	10.3320	9.8880	9.8880	10.0360	
¹ Impact - ambier	nt velocity.				

Table 62 Clark's Feri	ry, Pool El t	546.0, LCED29	, Run 2 Jun 9	5	
			Replicate		Return
Probe	А	В	C	AVG	Velocity' m/sec
1	0.2509	0.2389	0.2302	0.2400	
2	0.2361	0.2374	0.2267	0.2334	
3	0.3043	0.2922	0.2988	0.2984	
4	0.3454	0.3345	0.3481	0.3427	
5	0.3908	0.3774	0.3609	0.3764	
6	0.3954	0.3906	0.3873	0.3911	
7	0.3889	0.3927	0.3966	0.3927	
8	0.1592	0.0949	0.1234	0.1258	
		Impact Velocity	y, m/sec		
1	0.1272	0.0900	0.1307	0.1160	0.1240
2	0.0895	0.1359	0.1224	0.1159	0.1175
3	0.1364	0.1522	0.1154	0.1347	0.1637
4	0.1304	0.1422	0.1360	0.1362	0.2065
5	0.1363	0.1274	0.1338	0.1325	0.2439
6	0.2362	0.2172	0.2035	0.2190	0.1721
7	0.2440	0.1968	0.2545	0.2318	0.1609
8	-0.0833	0.0011	0.0209	-0.0204	0.1462
			Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	4.5870	4.4890	3.6760	4.2507	
171 m RB	2.9550	2.6790	4.9810	3.5383	
¹ Impact - ambiei	nt velocity.				

Table 63 Clark's Ferr	ry, Pool El 5	46.0, LCED38,	Run 5 Jun 95	5	
			Replicate		Return
Probe	A	В	с	AVG	Velocity' m/sec
1	0.2338	0.2316	0.2348	0.2334	
2	0.2495	0.2488	0.2480	0.2488	
3	0.2940	0.2901	0.2985	0.2942	
4	0.3422	0.3569	0.3454	0.3482	
5	0.3835	0.3683	0.3708	0.3742	
6	0.4233	0.4003	0.3924	0.4053	
7	0.4051	0.4035	0.4111	0.4066	
8	0.0943	0.0804	0.0918	0.0888	
		Impact Velocity	, m/sec		
1	0.0005	0.0000	0.0339	0.0115	0.2219
2	0.0501	0.0278	0.2480	0.1086	0.1402
3	0.0383	0.0257	0.2985	0.1208	0.1734
4	0.0485	0.0566	-0.0131	0.0307	0.3175
5	0.0377	0.0590	0.0426	0.0464	0.3278
6	0.1441	0.1484	0.1563	0.1496	0.2557
7	0.2024	0.1709	0.1661	0.1798	0.2268
8	-0.0396	-0.0018	-0.0015	-0.0143	0.1031
			Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	11.7870	10.0600	11.6480	11.1650	
171 m RB	4.5150	2.6990	3.9830	3.7320	
¹ Impact - ambie	nt velocity.				

Table 64 Clark's Ferry Pool 546.0 Conditions for Vertical Distribution Experiments										
Experiment No.	Up or Down	Tow Speed ¹ m/sec	Position ²	Temp ° C	Actual Draft m	Effective Draft ³ m	Barge W X L	Prop Thrust 1,000 lb	Schijf Velocity⁴ cm/sec	Schijf Drawdown⁴ cm
LCVUCD	U	3.18	252.7	22.0	2.13	2.67	3X5	108	24.2	8.9
LCVDCD	D	3.82	252.7	22.0	2.13	2.67	3X5	108	24.2	8.9
LCVUBE	U	3.18	252.7	22.0	2.13	2.67	3X5	108	24.2	8.9
LCVDBE	D	3.82	252.7	22.0	2.13	2.67	3X5	108	24.2	8.9
LCVUAF	U	3.18	252.7	22.0	2.13	2.67	3X5	108	24.2	8.9
LCVDAF	D	3.82	252.7	22.0	2.13	2.67	3X5	108	24.2	8.9
Note: Water	surface w	/idth 614 8	m area 2 170	sam Q6	90 cms w	ater surface e	elevation 5	46.0 avera	de ambient v	velocity

Note: Water surface width 614.8 m, area 2,170 sq m, Q 690 cms, water 0.32 m/sec, 26° rake. ¹ Relative to ground. ² Meters from right bank. ³ Actual draft + draft correction. ⁴ Schijf equation using effective draft and vessel speed relative to water. n, Q 690 cms, water surface elevation 546.0, aver 6 .8 n, a ag

Table 65 Clark's Fer	ry, Pool El 546	6.0, LCVDCD, F	Run 12 Jun 9	5, Vertical Distrib	ution
		_			
Depth off Bottom, %	А	В	с	AVG	Return Velocity ¹ m/sec
80	0.3901	0.4141	0.3986	0.4009	
50	0.3160	0.3160	0.3069	0.3130	
20	0.3620	0.3612	0.3534	0.3589	
		Impact Velocity, m	/sec		
80	0.0670	0.0569	0.0889	0.0709	0.3328
50	-0.0379	0.0248	-0.0150	-0.0094	0.3224
20	0.0585	0.0717	0.0534	0.0612	0.2977
		Dra	wdown, cm		
Distance from Thalweg m	A	в	с	AVG	
351 m LB	11.9630	10.6560	11.3330	11.3173	
234 m RB	10.6660	9.1850	9.5930	9.8147	
Note: Local wate ¹ Impact - ambie	er depth 5.0 m, LB 34 nt velocity.	1 m left of thalweg.			

Table 66 Clark's Feri	ry, Pool El 546	.0, LCVUCD, R	tun 13 Jun 95	, Vertical Distrib	ution
Depth off Bottom, %	A	В	с	AVG	Return Velocity ¹ m/sec
80	0.3932	0.3877	0.3969	0.3926	
50	0.3150	0.2936	0.3157	0.3081	
20	0.3481	0.3400	0.3600	0.3494	
		Impact Velocity, m/	/sec		
80	0.7559	0.7610	0.7743	0.7637	0.3711
50	0.6281	0.6759	0.7136	0.6725	0.3644
20	0.6702	0.6846	0.7126	0.6891	0.3397
		Dra	wdown, cm		
Distance from Thalweg m	A	В	с	AVG	
351 m LB	12.0000	11.9450	11.9450	11.9633	
234 m RB	13.0000	13.0560	13.1480	13.0680	
Note: Local wate	r depth 5.0 m, LB 34 nt velocity.	m left of thalweg.			

Table 67 Clark's Ferr	ry, Pool El 546	.0, LCVUBE, R	tun 14 Jun 95	, Vertical Distrib	ution
Depth off Bottom, %	А	В	с	AVG	Return Velocity ¹ m/sec
		Ambient Velocity, m	n/sec		
80	0.3158	0.3028	0.3040	0.3075	
50	0.2758	0.2724	0.2656	0.2713	
20	0.2558	0.2532	0.2485	0.2525	
		Impact Velocity, m/	/sec		
80	0.5881	0.6025	0.6009	0.5972	0.2897
50	0.5615	0.5874	0.5830	0.5773	0.3060
20	0.5391	0.5582	0.5507	0.5493	0.2968
		Dra	wdown, cm		
Distance from Thalweg m	A	в	c	AVG	
30 m LB	19.7140	20.5900	20.7360	20.3467	
30 m RB	15.3010	15.4410	15.8820	15.5413	
Note: Local wate ¹ Impact - ambier	r depth 5.0 m, LB 17 nt velocity.	2 m left of thalweg.			

Table 68 Clark's Fer	ry, Pool El 5	46.0, LCVDBE,	Run 14 Jun	95, Vertical Di	stribution
Depth off Bottom, %	A	в	с	AVG	Return Velocity ¹ m/sec
80	0.3130	0.3119	0.2959	0.3069	
50	0.2883	0.2757	0.2615	0.2752	
20	0.2627	0.2487	0.2385	0.2500	
		Impact Velocity,	m/sec		
80	0.0932	0.0917	0.0676	0.0842	0.2227
50	0.0684	0.0633	0.0308	0.0542	0.2210
20	0.0646	0.0492	0.0389	0.0509	0.1991
		C	Drawdown, cm		
Distance from Thalweg m	A	в	с	AVG	
30 m LB	16.0310	17.4360	17.5640	17.0103	
30 m RB	13.4740	17.1790	16.9220	15.8583	
Note: Local wate ¹ Impact - ambie	er depth 3.10 m, L nt velocity.	B 172 m left of thalwe	eg.		

Table 69 Clark's Fer	ry, Pool El 546	6.0, LCVUAF, R	un 16 Jun 95	, Vertical Distrib	ution
Depth off Bottom, %	A	В	с	AVG	Return Velocity¹ m/sec
80	0.2549	0.2593	0.2522	0.2555	
50	0.2664	0.2729	0.2711	0.2701	
20	0.1869	0.1976	0.1811	0.1885	
		Impact Velocity, m	/sec		
80	0.5849	0.5821	0.5780	0.5817	0.3262
50	0.5934	0.5701	0.5723	0.5768	0.3085
20	0.4795	0.4855	0.4738	0.4796	0.2911
		Dra	wdown, cm		
Distance from Thalweg m	A	в	с	AVG	
171 m LB	10.4630	11.0190	10.3330	10.6050	
138 m RB	9.2600	14.3520	8.8880	10.8333	
Note: Local wate ¹ Impact - ambie	er depth 2.64 m, LB 3 nt velocity.	318 m left of thalweg.			

Table 70 Clark's Feri	ry, Pool El 546	.0, LCVDAF, R	un 16 Jun 95	, Vertical Distrib	ution
Depth off Bottom, %	A	В	с	AVG	Return Velocity ¹ m/sec
		Ambient V	elocity, m/sec		
80	0.2590	0.2736	0.2528	0.2618	
50	0.2673	0.2807	0.2588	0.2689	
20	0.2060	0.2095	0.1976	0.2044	
		Impact Ve	locity, m/sec		
80	0.0434	0.0589	0.0763	0.0595	0.2023
50	0.0489	0.0174	0.0009	0.0224	0.2465
20	-0.0176	0.0079	0.0186	0.0030	0.2014
		Dra	wdown, cm		
Distance from Thalweg m	A	В	с	AVG	
171 m LB	16.2220	15.9260	15.2790	15.8090	
138 m RB	9.3330	9.0740	9.2130	9.2067	
Note: Local wate ¹ Impact - ambier	r depth 2.64 m, LB 3 nt velocity.	18 m left of thalweg.			

Table 71 Clark's Ferry Pool 551.5 Conditions										
Experiment No.	Up or Down	Tow Speed ¹ m/sec	Position ²	Temp ° C	Actual Draft m	Effective Draft ³ m	Barge W X L	Prop Thrust 1,000 lb	Schijf Velocity⁴ cm/sec	Schijf Drawdown⁴ cm
HCU138	U	1.38	256.9	26.0	2.13	2.73	3X5	54	5.3	1.0
HCU183	U	1.83	256.9	26.0	2.13	2.71	3X5	67.5	6.9	1.6
HCU228	U	2.28	256.9	26.0	2.13	2.69	3X5	81	8.7	2.4
HCU273	U	2.73	256.9	26.0	2.13	2.67	3X5	94.5	10.8	3.5
HCU318	U	3.18	256.9	26.0	2.13	2.65	3X5	108	13.4	5.0
HCU416	U	4.16	256.9	26.0	2.13	2.63	3X5	135	22.6	10.8
				-		-	_			
HCD202	D	2.02	256.9	26.0	2.13	2.76	3X5	54	4.8	0.8
HCD247	D	2.47	256.9	26.0	2.13	2.73	3X5	67.5	6.4	1.4
HCD292	D	2.92	256.9	26.0	2.13	2.70	3X5	81	8.1	2.1
HCD337	D	3.37	256.9	26.0	2.13	2.68	3X5	94.5	10.0	3.1
HCD382	D	3.82	256.9	26.0	2.13	2.67	3X5	108	12.5	4.4
HCD477	D	4.77	256.9	26.0	2.13	2.64	3X5	135	20.2	9.2
					_					

Note: Water surface width 627 m, area 3,215 sq m, Q 1,285 cms, water surface elevation 551.5, 26° rake. ¹ Relative to ground. ² Meters from right bank. ³ Actual draft + draft correction. ⁴ Schijf equation using effective draft and vessel speed relative to water.

Table 72 Clark's Ferr	ry, Pool El 5	51.5, HCU138	, Run 4 Aug 9	5				
		Return						
Probe	А	В	С	AVG	Velocity ¹ m/sec			
1	0.3202	0.3398	0.3377	0.3326				
2	0.3595	0.3672	0.3692	0.3653				
3	0.4393	0.4214	0.4495	0.4367				
4	0.4362	0.4398	0.4454	0.4405				
5	0.4421	0.4829	0.4825	0.4692				
6	0.5024	0.5067	0.5047	0.5046				
7	0.4057	0.3785	0.4184	0.4009				
8	0.1714	0.1738	0.1847	0.1766				
	Impact Velocity, m/sec							
1	0.4397	0.4350	0.4173	0.4307	0.1001			
2	0.4673	0.4768	0.4525	0.4655	0.1002			
3	0.5278	0.5139	0.5447	0.5288	0.0921			
4	0.5719	0.5486	0.5847	0.5684	0.1279			
5	0.5910	0.5995	0.6148	0.6018	0.1326			
6	0.5465	0.6111	0.6129	0.5902	0.0856			
7	0.4749	0.4975	0.4662	0.4795	0.0786			
8	0.3607	0.3581	0.3761	0.3650	0.1884			
			Drawdown, cm					
Distance from Thalweg m	A	В	c	AVG				
186 m LB	1.2500	1.7500	1.5000	1.5000				
180 m RB	0.5500	0.7550	0.6500	0.6517				
¹ Impact - ambie	nt velocity.				· · · · ·			

Table 73 Clark's Feri	ry, Pool El 5	551.5, HCU183	, Run 3 Aug 9	5	
		Return			
Probe	A	В	С	AVG	Velocity' m/sec
		Ambier	nt Velocity, m/sec		
1	0.3589	0.3435	0.3282	0.3435	
2	0.3743	0.3684	0.3737	0.3721	
3	0.4249	0.4542	0.4290	0.4360	
4	0.4471	0.4400	0.4302	0.4391	
5	0.4412	0.4468	0.4715	0.4532	
6	0.4751	0.4814	0.4900	0.4822	
7	0.4014	0.3696	0.4077	0.3929	
8	0.1344	0.1277	0.2517	0.1713	
		Impac	t Velocity, m/sec		
1	0.4281	0.4417	0.4237	0.4312	0.0877
2	0.4735	0.4607	0.4777	0.4706	0.0985
3	0.5519	0.5366	0.5303	0.5396	0.1036
4	0.5901	0.6361	0.6134	0.6132	0.1741
5	0.6679	0.6479	0.6577	0.6578	0.2046
6	0.5880	0.5934	0.5815	0.5876	0.1054
7	0.4655	0.4768	0.4704	0.4709	0.0780
8	0.3551	0.3396	0.3679	0.3542	0.1829
			Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	2.7500	2.9300	2.6000	2.7600	
180 m RB	1.1000	0.9890	1.2000	1.0963	
¹ Impact - ambier	nt velocity.				

Table 74 Clark's Ferr	ry, Pool El 5	551.5, HCU228,	, Run 3 Aug 9	5	
		Return			
Probe	А	В	с	AVG	Velocity' m/sec
1	0.3651	0.3643	0.3416	0.3570	
2	0.3800	0.3696	0.3802	0.3766	
3	0.4319	0.4302	0.4303	0.4308	
4	0.4287	0.4217	0.4371	0.4292	
5	0.4703	0.4716	0.4596	0.4672	
6	0.4932	0.4882	0.4758	0.4857	
7	0.3770	0.3745	0.3748	0.3754	
8	0.1668	0.0941	0.1762	0.1457	
1	0.4148	0.4177	0.4472	0.4266	0.0696
2	0.5042	0.4911	0.4718	0.4890	0.1124
3	0.5250	0.5366	0.5642	0.5419	0.1111
4	0.6241	0.6333	0.6133	0.6236	0.1944
5	0.6129	0.6216	0.6087	0.6144	0.1472
6	0.6014	0.5771	0.6216	0.6000	0.1143
7	0.4750	0.4814	0.4834	0.4799	0.1045
8	0.2934	0.3776	0.2974	0.3228	0.1771
	·		Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	4.2000	4.7500	4.6300	4.5267	
180 m RB	2.0500	2.3000	2.3890	2.2463	
¹ Impact - ambie	nt velocity.				

Table 75 Clark's Fer	ry, Pool El 🤅	551.5, HCU273	, Run 3 Aug 9	5				
		Return						
Probe	А	В	С	AVG	Velocity ¹ m/sec			
1	0.3387	0.3137	0.3361	0.3295				
2	0.3422	0.3413	0.3861	0.3565				
3	0.4449	0.4404	0.4298	0.4384				
4	0.4053	0.4375	0.4544	0.4324				
5	0.4632	0.4540	0.4574	0.4582				
6	0.5074	0.5024	0.4874	0.4991				
7	0.3937	0.4055	0.4083	0.4025				
8	0.1082	0.1464	0.0946	0.1164				
	Impact Velocity, m/sec							
1	0.4645	0.4042	0.4337	0.4341	0.1046			
2	0.4772	0.4449	0.4850	0.4690	0.1125			
3	0.6042	0.5844	0.5452	0.5779	0.1395			
4	0.6928	0.6523	0.6487	0.6646	0.2322			
5	0.6331	0.6357	0.6981	0.6556	0.1974			
6	0.6035	0.6622	0.6339	0.6332	0.1341			
7	0.4743	0.4873	0.4811	0.4809	0.0784			
8	0.2868	0.3766	0.2895	0.3176	0.2012			
	·	<u>.</u>	Drawdown, cm	<u>.</u>				
Distance from Thalweg m	A	В	c	AVG				
186 m LB	5.9050	5.6860	5.8290	5.8067				
180 m RB	3.1740	2.8570	2.9710	3.0007				
¹ Impact - ambie	nt velocity.				·			

Table 76 Clark's Ferry, Pool El 551.5, HCU318, Run 2 Aug 95					
	Replicate				Return
Probe	А	В	с	AVG	Velocity' m/sec
	Ambient Velocity, m/sec				
1	0.3250	0.3433	0.3480	0.3388	
2	0.3668	0.3433	0.3590	0.3564	
3	0.4260	0.3650	0.4413	0.4108	
4	0.4443	0.4112	0.4444	0.4333	
5	0.4658	0.4255	0.4488	0.4467	
6	0.4699	0.4467	0.4574	0.4580	
7	0.3657	0.3740	0.3864	0.3754	
8	0.1291	0.1686	0.1663	0.1547	
	Impact Velocity, m/sec				
1	0.4194	0.4713	0.5035	0.4647	0.1259
2	0.5167	0.4713	0.5080	0.4987	0.1423
3	0.6120	0.5412	0.6207	0.5913	0.1805
4	0.6845	0.5992	0.6998	0.6612	0.2279
5	0.6440	0.6589	0.6827	0.6619	0.2152
6	0.6603	0.6461	0.6807	0.6624	0.2044
7	0.5370	0.5295	0.5209	0.5291	0.1537
8	0.3649	0.3027	0.2009	0.2895	0.1348
Drawdown, cm					
Distance from Thalweg m	A	В	c	AVG	
186 m LB	9.9300	8.8390	9.5550	9.4413	
180 m RB	6.1780	5.8930	5.3330	5.8013	
¹ Impact - ambient velocity.					
Table 77 Clark's Ferr	ry, Pool El 55	51.5, HCU416, R	un 4 Aug 95		
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		Re	plicate		Return
Probe	А	В	с	AVG	Velocity' m/sec
1	0.3261	0.3533	0.3500	0.3431	
2	0.3662	0.3688	0.3756	0.3702	
3	0.4445	0.4619	0.4422	0.4495	
4	0.4279	0.4187	0.4315	0.4260	
5	0.4184	0.4318	0.4533	0.4345	
6	0.4643	0.4803	0.4935	0.4794	
7	0.3915	0.3871	0.3922	0.3903	
8	0.1427	0.1695	0.2300	0.1807	
1	0.5438	0.5619	0.5470	0.5509	0.2078
2	0.5825	0.6212	0.6222	0.6086	0.2384
3	0.6636	0.6889	0.6670	0.6732	0.2237
4	0.8056	0.7789	0.7373	0.7739	0.3479
5	0.6913	0.7035	0.7035	0.6994	0.2649
6	0.6771	0.6672	0.6614	0.6686	0.1891
7	0.5791	0.5862	0.5914	0.5856	0.1953
8	0.3976	0.3809	0.3201	0.3662	0.1855
		Dra	awdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	16.6250	17.3750	16.6250	16.8750	
180 m RB	9.3130	9.1250	9.3130	9.2503	
¹ Impact - ambie	nt velocity.				

Table 78 Clark's Feri	ry, Pool El 5	51.5, HCD202, R	un 31 Jul 95		
		Re	plicate		Return
Probe	A	В	с	AVG	Velocity' m/sec
1	0.3331	0.3272	0.3399	0.3334	
2	0.3816	0.3630	0.3708	0.3718	
3	0.4134	0.4083	0.4335	0.4184	
4	0.4561	0.4349	0.4576	0.4495	_
5	0.4694	0.4638	0.4563	0.4632	_
6	0.4855	0.5176	0.4541	0.4857	_
7	0.3835	0.3532	0.3704	0.3690	_
8	0.1208	0.1529	0.1456	0.1398	
	·				
1	0.2763	0.2697	0.3058	0.2839	0.0495
2	0.3013	0.3193	0.3111	0.3106	0.0612
3	0.3204	0.3541	0.3387	0.3377	0.0807
4	0.3569	0.3347	0.3399	0.3438	0.1057
5	0.3379	0.3049	0.3167	0.3198	0.1434
6	0.4095	0.3647	0.3939	0.3894	0.0963
7	0.3216	0.3194	0.2842	0.3084	0.0606
8	0.1208	0.1529	0.1456	0.1398	0.0000
		Dra	awdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB					
180 m RB					
¹ Impact - ambier	nt velocity.			·	

Table 79 Clark's Ferr	ry, Pool El S	551.5, HCD247	Run 31 Jul 9	5	
			Replicate		Return
Probe	А	В	с	AVG	Velocity' m/sec
1	0.2979	0.3413	0.3339	0.3244	
2	0.3310	0.3598	0.3943	0.3617	
3	0.4219	0.4356	0.4057	0.4235	
4	0.4425	0.4704	0.4366	0.4498	
5	0.4614	0.4213	0.4251	0.4359	
6	0.4904	0.4791	0.4705	0.4800	
7	0.3527	0.3846	0.3712	0.3695	
8	0.2000	0.1996	0.2334	0.2110	
1	0.2159	0.2762	0.2539	0.2487	0.0757
2	0.2673	0.3073	0.3359	0.3035	0.0582
3	0.3734	0.3372	0.3349	0.3485	0.0750
4	0.3048	0.3278	0.3045	0.3124	0.1374
5	0.2596	0.2833	0.3324	0.2918	0.1441
6	0.3719	0.3678	0.3613	0.3670	0.1130
7	0.3527	0.2530	0.2994	0.3017	0.0678
8	0.2000	-0.1100	0.0477	0.0459	0.2619
			Drawdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	2.0000	1.5000	2.0000	1.8333	
180 m RB	1.5000	1.5000	1.5000	1.5000	
¹ Impact - ambie	nt velocity.				

Table 80 Clark's Feri	ry, Pool El 5	51.5, HCD292, F	≀un 1 Aug 95		
		Re	plicate		Return
Probe	A	В	С	AVG	Velocity' m/sec
1	0.3243	0.3229	0.3430	0.3301	
2	0.3682	0.3668	0.3715	0.3688	
3	0.4243	0.4030	0.4207	0.4160	
4	0.4146	0.4404	0.4509	0.4353	
5	0.4601	0.4521	0.4592	0.4571	
6	0.4887	0.4792	0.4768	0.4816	
7	0.3891	0.3987	0.3826	0.3901	
8	0.1632	0.2274	0.0827	0.1578	
1	0.2746	0.2777	0.2571	0.2698	0.0603
2	0.2963	0.3181	0.3159	0.3101	0.0587
3	0.3519	0.3615	0.3171	0.3435	0.0725
4	0.2737	0.3149	0.3181	0.3056	0.1297
5	0.3030	0.2566	0.2690	0.2762	0.1809
6	0.3171	0.3502	0.3194	0.3289	0.1527
7	0.3368	0.2725	0.2754	0.2949	0.0952
8	0.0385	0.0467	-0.0456	0.0132	0.1446
	<u> </u>	Dra	awdown, cm		<u> </u>
Distance from Thalweg m	A	В	с	AVG	
186 m LB	3.2180	2.5710	2.7860	2.8583	
180 m RB	3.5210	3.0000	4.0000	3.5070	
¹ Impact - ambier	nt velocity.				

Table 81 Clark's Feri	ry, Pool El 5	51.5, HCD337, R	un 2 Aug 95		
		Re	plicate		Return
Probe	A	В	с	AVG	Velocity' m/sec
1	0.3291	0.3538	0.3123	0.3317	
2	0.3736	0.3619	0.3472	0.3609	
3	0.4212	0.3984	0.4292	0.4163	
4	0.4409	0.4352	0.4401	0.4387	
5	0.4499	0.4622	0.4495	0.4539	
6	0.4751	0.5104	0.5080	0.4978	
7	0.3792	0.3893	0.3807	0.3831	
8	0.1768	0.1779	0.1662	0.1736	
	<u> </u>				
1	0.2682	0.2604	0.2376	0.2554	0.0763
2	0.2913	0.2564	0.2827	0.2768	0.0841
3	0.2953	0.3471	0.3058	0.3161	0.1002
4	0.3156	0.2382	0.2682	0.2740	0.1647
5	0.2228	0.2827	0.2884	0.2646	0.1893
6	0.3436	0.3298	0.3175	0.3303	0.1675
7	0.2690	0.2817	0.2805	0.2771	0.1060
8	0.0880	0.0270	0.0635	0.0595	0.1141
		Dra	awdown, cm	<u> </u>	
Distance from Thalweg m	A	В	с	AVG	
186 m LB	4.6000	4.3500	4.2250	4.3917	
180 m RB	3.7500	4.0500	3.8000	3.8667	
¹ Impact - ambier	nt velocity.				

Table 82 Clark's Fer	ry, Pool El {	551.5, HCD382	, Run 2 Aug 9	5	
			Return		
Probe	А	В	С	AVG	Velocity ¹ m/sec
1	0.3151	0.3033	0.3041	0.3075	
2	0.3614	0.3537	0.3547	0.3566	
3	0.4264	0.4426	0.4279	0.4323	
4	0.4315	0.4240	0.4258	0.4271	
5	0.4172	0.4487	0.4611	0.4423	
6	0.4916	0.4885	0.4913	0.4905	
7	0.3646	0.3715	0.3749	0.3703	
8	0.2148	0.0981	0.2418	0.1849	
1	0.2366	0.1898	0.2149	0.2138	0.0937
2	0.2569	0.2828	0.2356	0.2584	0.0982
3	0.2832	0.2724	0.2920	0.2825	0.1498
4	0.2519	0.2653	0.2408	0.2527	0.1744
5	0.1837	0.2248	0.2320	0.2135	0.2288
6	0.2878	0.2569	0.3040	0.2829	0.2076
7	0.2765	0.2596	0.1852	0.2404	0.1299
8	0.0103	-0.0805	-0.0165	-0.0289	0.2138
			Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	5.7500	4.8240	5.8860	5.4867	
180 m RB	4.6870	4.7340	4.7990	4.7400	
¹ Impact - ambie	nt velocity.				

Table 83 Clark's Feri	ry, Pool El 5	51.5, HCD477,	Run 2 Aug 9	5				
			Replicate		Return			
Probe	A	В	С	AVG	Velocity' m/sec			
	Ambient Velocity, m/sec							
1	0.3487	0.3279	0.3300	0.3355				
2	0.3493	0.3680	0.3835	0.3669				
3	0.4200	0.4480	0.4487	0.4389				
4	0.4570	0.4487	0.4345	0.4467				
5	0.4517	0.4643	0.4588	0.4583				
6	0.4881	0.4586	0.4746	0.4738				
7	0.4000	0.4048	0.3903	0.3984				
8	0.2065	0.2334	0.1945	0.2115				
1	0.1615	0.1731	0.1906	0.1751	0.1604			
2	0.2348	0.2396	0.2303	0.2349	0.1320			
3	0.2413	0.2607	0.2543	0.2521	0.1868			
4	0.2214	0.1844	0.2405	0.2154	0.2313			
5	0.2090	0.2016	0.2252	0.2119	0.2464			
6	0.2647	0.2815	0.3102	0.2855	0.1883			
7	0.1548	0.1971	0.1455	0.1658	0.2326			
8	0.0649	0.0677	0.0537	0.0621	0.1494			
		I	Drawdown, cm					
Distance from Thalweg m	A	В	с	AVG				
186 m LB	11.0870	11.6300	11.6300	11.4900				
180 m RB	9.4020	9.6740	5.6500	8.2420				
¹ Impact - ambier	nt velocity.							

Table 84 Clark's Ferry, Pool El 551.5, Experiments, Meter Positions

, ,								
		Probe Number						
Probe Position ¹ Experiment o.	1	2	3	4	5	6	7	8
PP1 (HCU138, HCU183, HCU228, HCU273, HCU318, HCU416, HCD202, HCD247, HCD292, HCD292, HCD337, HCD382, HCD477)	321.0 Left	228.0 Left	129.0 Left	30.0 Left	30.0 Right	99.0 Right	168.0 Right	237.0 Right
¹ Probe position, dis	tance in mete	rs from thalwe	eg, looking do	ownstream.				

Table 85 Clark's Ferry Pool 551.5 Experiment Conditions for Dikes										
Experiment No.	Up or Down	Tow Speed ¹ m/sec	Position ²	Temp ° C	Actual Draft m	Effective Draft ³ m	Barge W X L	Prop Thrust 1,000 lb	Schijf Velocity⁴ cm/sec	Schijf Drawdown⁴ cm
H59D29	D	2.92	256.9	26.0	2.13	2.70	3X5	81	8.1	2.1
H59D47	D	4.77	256.9	26.0	2.13	2.64	3X5	135	20.3	9.2
H59U22	U	2.28	256.9	26.0	2.13	2.69	3X5	81	8.7	2.4
H59U41	U	4.16	256.9	26.0	2.13	2.63	3X5	135	22.6	10.8
H59U22 H59U41	U U	2.28 4.16	256.9 256.9	26.0 26.0	2.13 2.13	2.69 2.63	3X5 3X5	81 135	8.7 22.6	2.4 10

Note: Water surface width 627 m, area 3,215 sq m, Q 1,285 cms, water surface elevation 541.5, 26° rake.

Relative to ground.

² Meters from right bank.
³ Actual draft + draft correction.
⁴ Schijf equation using effective draft and vessel speed relative to water.

Table 86 Clark's Fer	ry, Pool El	551.5, H59D29	, Run 7 Aug 9	5	
			Replicate		Return
Probe	А	В	С	AVG	Velocity' m/sec
1	0.3534	0.3508	0.3557	0.3533	
2	0.3708	0.3710	0.3873	0.3764	
3	0.5586	0.5738	0.5762	0.5695	
4	0.4815	0.4748	0.4766	0.4776	
5	0.4590	0.4483	0.4467	0.4513	
6	0.5009	0.4881	0.5108	0.4999	
7	0.3867	0.3945	0.3983	0.3932	
8	0.1395	0.1295	0.1328	0.1339	
1	0.3091	0.3001	0.2852	0.2981	0.0552
2	0.2929	0.3084	0.3376	0.3130	0.0634
3	0.4685	0.4960	0.4786	0.4810	0.0885
4	0.3106	0.2399	0.2965	0.2823	0.1953
5	0.3143	0.3242	0.3100	0.3162	0.1351
6	0.3217	0.3699	0.3637	0.3518	0.1481
7	0.2919	0.2992	0.2930	0.2947	0.0985
8	0.1395	0.1295	0.1328	0.1339	0.0000
		·	Drawdown, cm	·	
Distance from Thalweg m	A	В	c	AVG	
186 m LB	3.6250	0.3750	3.6880	3.6877	
180 m RB	4.1250	3.5000	4.1250	3.9167	
¹ Impact - ambie	nt velocity.				

Table 87 Clark's Feri	ry, Pool El 5	51.5, H59D47,	Run 7 Aug 95	5			
	Replicate						
Probe	A	В	С	AVG	Velocity' m/sec		
1	0.3601	0.3669	0.3490	0.3587			
2	0.3802	0.3927	0.3768	0.3832			
3	0.5641	0.5847	0.5830	0.5773			
4	0.4383	0.4716	0.4770	0.4623			
5	0.4970	0.4434	0.4388	0.4597			
6	0.3890	0.5061	0.4591	0.4514			
7	0.3837	0.3985	0.4664	0.4162			
8	0.3669	0.1198	0.0700	0.1856			
1	0.2136	0.1807	0.2098	0.2014	0.1573		
2	0.2417	0.2274	0.2453	0.2381	0.1451		
3	0.3495	0.2864	0.2789	0.3049	0.2724		
4	0.1627	0.2820	0.2331	0.2259	0.2364		
5	0.3364	0.1942	0.2209	0.2505	0.2092		
6	0.1768	0.3061	0.1858	0.2229	0.2285		
7	-0.0173	0.2441	0.1640	0.1303	0.2859		
8	0.3669	0.1198	0.0700	0.1856	0.0000		
		ŀ	Drawdown, cm				
Distance from Thalweg m	A	В	с	AVG			
186 m LB	9.3550	10.4840	13.2260	11.0217			
180 m RB	9.0490	10.0000	9.5170	9.5219			
¹ Impact - ambier	nt velocity.						

Table 88 Clark's Fer	ry, Pool El 5	551.5, H59U22,	Run 16 Aug	95	
			Replicate		Return
Probe	А	В	С	AVG	Velocity' m/sec
1	0.3573	0.3478	0.3650	0.3567	
2	0.3490	0.3589	0.3525	0.3535	
3	0.5490	0.5185	0.5746	0.5474	
4	0.4719	0.4301	0.4516	0.4512	
5	0.4285	0.4586	0.4330	0.4400	
6	0.4693	0.4638	0.4620	0.4650	
7	0.3906	0.3776	0.3790	0.3824	
8	0.0153	0.0829	0.0280	0.0421	
1	0.4297	0.4363	0.4212	0.4291	0.0724
2	0.4632	0.4594	0.4741	0.4656	0.1121
3	0.7202	0.6831	0.7035	0.7023	0.1549
4	0.5101	0.5538	0.5166	0.5268	0.0756
5	0.6036	0.5566	0.5483	0.5695	0.1295
6	0.5566	0.5740	0.5919	0.5742	0.1092
7	0.4738	0.4401	0.4611	0.4583	0.0759
8	0.3123	0.3586	0.3380	0.3363	0.2942
			Drawdown, cm		
Distance from Thalweg m	A	В	c	AVG	
186 m LB	2.6960	3.6780	3.5640	3.3127	
180 m RB	2.2170	2.7510	2.5360	2.5013	
¹ Impact - ambie	nt velocity.				· · · ·

Table 89 Clark's Ferry, Pool El 551.5, H59U41, Run 16 Aug 95						
	Return					
Probe	А	в	с	AVG	Velocity ¹ m/sec	
		Ambien	t Velocity, m/sec			
1	0.3563	0.3498	0.3726	0.3596		
2	0.3629	0.3589	0.3507	0.3575		
3	0.5559	0.5609	0.5541	0.5570		
4	0.4318	0.4735	0.4374	0.4476		
5	0.4301	0.4157	0.4127	0.4195		
6	0.4565	0.4771	0.4422	0.4586		
7	0.3933	0.3661	0.3677	0.3757		
8	-0.0232	0.0719	0.0540	0.0342		
		Impact	Velocity, m/sec			
1	0.5441	0.5457	0.5278	0.5392	0.1796	
2	0.5659	0.5530	0.5478	0.5556	0.1981	
3	0.8822	0.9008	0.8702	0.8844	0.3274	
4	0.5239	0.7857	0.7899	0.6998	0.2522	
5	0.6257	0.6415	0.6569	0.6414	0.2219	
6	0.6382	0.6561	0.6005	0.6316	0.1730	
7	0.5290	0.5524	0.5255	0.5356	0.1599	
8	0.4118	0.4611	0.2778	0.3836	0.3494	
			Drawdown, cm			
Distance from Thalweg m	A	В	c	AVG		
186 m LB	11.8190	12.4550	11.1820	11.8187		
180 m RB	6.8180	6.7270	6.7270	6.7573		
¹ Impact - ambier	nt velocity.					

Table 90 Clark's Ferry Pool 572.7 Experiment Conditions

	Glark 51 erry 1 oor 572.7 Experiment Conditions									
Experiment No.	Up or Down	Tow Speed ¹ m/sec	Position ²	Temp ° C	Actual Draft m	Effective Draft ³ m	Barge W X L	Prop Thrust 1,000 lb	Schijf Velocity⁴ cm/sec	Schijf Drawdown⁴ cm
CHU228	U	2.28	259.1	24.0	2.13	2.69	3X5	81	3.2	0.8
CHU318	U	3.18	259.1	24.0	2.13	2.66	3X5	108	4.4	1.5
CHU408	U	4.08	259.1	24.0	2.13	2.64	3X5	135	6.2	2.8
CHD292	D	2.92	259.1	24.0	2.13	2.69	3X5	81	3.5	1.0
CHD382	D	3.82	259.1	24.0	2.13	2.66	3X5	108	4.7	1.7
CHD472	D	4.77	259.1	24.0	2.13	2.64	3X5	135	6.5	3.0

Note: Water surface width 629.5 m, area 7,283 sq m, water surface elevation 572.7, 26° rake. ¹ Relative to ground. ² Meters from right bank. ³ Actual draft + draft correction. ⁴ Schijf equation using effective draft and vessel speed relative to water.

Table 91 Clark's Fer	ry, Pool El 🤅	572.7, CHU228	, Run 8 Sep 9	5	
		Return			
Probe	А	в	с	AVG	Velocity' m/sec
		Ambie	nt Velocity, m/sec		
1	0.1751	0.1456	0.1149	0.1452	
2	0.3792	0.2993	0.1602	0.2796	
3	0.4225	0.3554	0.1625	0.3135	
4	0.2491	0.2545	0.1267	0.2101	
5	0.2343	0.3068	0.2116	0.2509	
6	0.2569	0.2889	0.2084	0.2514	
7	0.4340	0.2550	0.1905	0.1630	
8		0.3269	0.1470	0.2370	
		Impac	t Velocity, m/sec	L	
1	0.2652	0.2660	0.1149	0.2150	0.0700
2	0.3792	0.2993	0.1602	0.2796	0.0000
3	0.4225	0.4669	0.1625	0.3506	0.0370
4	0.2491	0.2545	0.3542	0.2859	0.0760
5	0.3249	0.3234	0.2870	0.3118	0.0610
6	0.3492	0.3637	0.2957	0.3362	0.0850
7	0.0434	0.3661	0.1905	0.2000	0.0370
8		0.3269	0.1470	0.2370	0.0000
		<u> </u>	Drawdown, cm	<u> </u>	
Distance from Thalweg m	A	В	c	AVG	
186 m LB	1.0000	1.0000	1.2500	1.0833	
171 m RB	1.0000	0.7500	1.0000	0.9167	
¹ Impact - ambie	nt velocity.				

Table 92 Clark's Feri	ry, Pool El 572	2.7, CHU318, R	un 8 Sep 95		
			Return		
Probe	Α	В	С	AVG	Velocity' m/sec
		Ambient Ve	elocity, m/sec		
1	0.1148	0.0775	0.1139	0.1021	
2	0.1445	0.1056	0.1482	0.1328	
3	0.1446	0.1228	0.1190	0.1288	
4	0.1188	0.1667	0.1337	0.1397	
5	0.2342	0.2412	0.2327	0.2360	
6	0.2417	0.3123	0.2093	0.2544	
7	0.2100	0.2011	0.1719	0.1943	
8					
		Impact Ve	locity, m/sec		
1	0.1148	0.1308	0.1139	0.1198	0.0180
2	0.1886	0.1511	0.1855	0.1751	0.0420
3	0.2618	0.2145	0.2188	0.2317	0.1030
4	0.2889	0.3700	0.2479	0.3023	0.1630
5	0.2882	0.3159	0.3007	0.3016	0.0660
6	0.3412	0.3610	0.3333	0.3542	0.0910
7	0.2907	0.2840	0.2144	0.2630	0.0690
8					
		Dra	wdown, cm		
Distance from Thalweg m	A	в	с	AVG	
186 m LB	2.0000	1.5000	1.7500	1.7500	
171 m RB	2.0000	2.0000	1.0000	1.6667	
¹ Impact - ambier	nt velocity.				

Table 93 Clark's Feri	ry, Pool El 572	2.7, CHU408, R	un 11 Sep 95		
			Return		
Probe	Α	В	с	AVG	Velocity' m/sec
		Ambient V	elocity, m/sec		
1	0.1897	0.1859	0.1795	0.1850	
2	0.2657	0.2588	0.3163	0.2803	
3	0.3310	0.3181	0.2870	0.3120	
4	0.3480	0.3473	0.2841	0.3265	
5	0.3321	0.2648	0.2607	0.2859	
6	0.3031	0.2646	0.2813	0.2830	
7	0.2710	0.3182	0.3525	0.3139	
8	0.2189	0.1955	0.0276	0.1473	
		Impact Ve	locity, m/sec	·	
1	0.2387	0.2723	0.2455	0.2522	0.0670
2	0.3212	0.3407	0.3021	0.3213	0.0410
3	0.4602	0.4833	0.3465	0.4300	0.1180
4	0.3962	0.3302	0.2841	0.3368	0.0100
5	0.3998	0.3801	0.3374	0.3724	0.0870
6	0.3711	0.3861	0.3627	0.3733	0.0900
7	0.3456	0.3665	0.3861	0.3661	0.0520
8	0.2189	0.1955	0.0276	0.1473	0.0000
		Dra	wdown, cm		·
Distance from Thalweg m	A	В	с	AVG	
186 m LB	3.6670	4.1930	4.0000	3.9533	
171 m RB	2.9030	3.2900	3.3720	3.1883	
¹ Impact - ambier	nt velocity.				

Table 94 Clark's Feri	ry, Pool El 5	72.7, CHD292,	Run 6 Sep 9	5	
		Return			
Probe	А	В	с	AVG	Velocity' m/sec
		Ambient	t Velocity, m/sec		
1	0.0865	0.1090	0.1222	0.1059	
2	0.1350	0.1704	0.1611	0.1555	
3	0.1728	0.1546	0.1364	0.1546	
4	0.1026	0.1689	0.0947	0.1221	
5	0.2206	0.1896	0.1896	0.1990	
6	0.2392	0.2371	0.2270	0.2344	
7	0.1588	0.1671	0.1431	0.1563	
8	0.2987			0.2987	
		Impact	Velocity, m/sec		
1	0.0865	0.1090	0.1222	0.1059	0.0000
2	0.1350	0.1704	0.1611	0.1555	0.0000
3	0.1728	0.1546	0.0255	0.1176	0.0370
4	0.1026	0.1689	0.0947	0.1221	0.0000
5	0.1415	0.1433	0.1265	0.1371	0.0620
6	0.2392	0.1457	0.1239	0.1696	0.0650
7	0.1588	0.0800	0.0612	0.1000	0.0563
8	0.2987			0.2987	0.0000
		D	Drawdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	1.0000	1.0000	1.2500	1.0833	
171 m RB	1.0000	1.2000	1.5000	1.2333	
¹ Impact - ambier	nt velocity.				

Table 95 Clark's Feri	ry, Pool El 572	2.7, CHD382, R	un 7 Sep 95		
			Return		
Probe	А	В	с	AVG	Velocity' m/sec
		Ambient V	elocity, m/sec		
1	0.2172	0.2720	0.2279	0.2390	
2	0.3232	0.3495	0.2454	0.3060	
3	0.2773	0.3387	0.4155	0.3438	
4	0.2672	0.3186	0.3181	0.3013	
5	0.2963	0.2388	0.2731	0.2694	
6	0.3331	0.2299	0.2726	0.2785	
7	0.2186	0.2098	0.1627	0.1970	
8					
		Impact Ve	locity, m/sec		
1	0.2172	0.2213	0.2279	0.2221	0.0170
2	0.2403	0.2998	0.2454	0.2618	0.0440
3	0.2773	0.2267	0.2521	0.2520	0.0920
4	0.2672	0.1002	0.0751	0.1475	0.1540
5	0.1990	0.1642	0.1975	0.1869	0.0830
6	0.2387	0.1851	0.1785	0.2008	0.0780
7	0.1565	0.1474	0.0706	0.1248	0.0720
8					
		Dra	wdown, cm		
Distance from Thalweg m	A	В	с	AVG	
186 m LB	2.4300	2.9310	2.5600	2.6403	
171 m RB	1.7590	2.4480	2.2000	2.1357	
¹ Impact - ambier	nt velocity.				

Table 96 Clark's Feri	ry, Pool El 572	2.7, CHD472, R	un 7 Sep 95		
			Return		
Probe	А	В	с	AVG	Velocity' m/sec
		Ambient V	elocity, m/sec		
1	0.2393	0.2058	0.2078	0.2176	
2	0.3036	0.3532	0.3336	0.3301	
3	0.3496	0.3152	0.3402	0.3350	
4	0.2953	0.2446	0.2880	0.2760	
5	0.2684	0.2876	0.2562	0.2707	
6	0.3352	0.2323	0.2277	0.2651	
7	0.2152	0.1838	0.1880	0.1957	
8					
		Impact Ve	locity, m/sec	·	
1	0.2393	0.2058	0.2078	0.2176	0.0000
2	0.3036	0.2939	0.2795	0.2923	0.0380
3	0.1965	0.2213	0.2061	0.2080	0.1270
4	0.0702	-0.1077	0.0307	-0.0023	0.2780
5	0.1836	0.1697	0.1693	0.1742	0.0970
6	0.1832	0.1294	0.2277	0.1801	0.0850
7	0.1253	0.1517	0.1342	0.1371	0.0590
8					
		Dra	wdown, cm		·
Distance from Thalweg m	A	В	с	AVG	
186 m LB	3.6430	4.1960	3.7110	3.8500	
171 m RB	3.4640	3.9280	3.7740	3.7220	
¹ Impact - ambier	nt velocity.				

Table 97 Clark's Ferry Pool 551.5 Drawdown Experiment Conditions										
Experiment No.	Up or Down ¹	Tow Speed ² m/sec	Position ³	Temp ° C	Actual Draft m	Effective Draft⁴ m	Barge W X L	Prop Thrust 1,000 lb	Schijf Velocity⁵ cm/sec	Schijf Drawdown⁵ cm
CHF260	-	2.60	256.9	9.0	2.13	2.75	3X5	81	8.6	2.3
CHF350	-	3.50	256.9	9.0	2.13	2.71	3X5	108	13.2	4.8
CHF376	-	3.76	256.9	9.0	2.13	2.70	3X5	135	15.0	5.9
Note: Water s ¹ Slack water. ² Relative to gr ³ Meters from ⁴ Actual draft -	2HF376 - 3.76 256.9 9.0 2.13 2.70 3X5 135 15.0 5.9 Vote: Water surface width 627 m, area 3,215 sq m, water surface elevation 551.5, 26° rake. Slack water. Slack water. Slack water. Relative to ground. Meters from right bank. Activel draft correction Slack water.									

⁵ Schijf equation using effective draft and vessel speed relative to water.

Table 98 Clark's Ferry, Pool El 551.5, CHF260, Run 2 Jan 96								
		Drawdown, cm						
		Rep	olicate					
Distance from Thalweg m	A	В	с	AVG				
30 m RB	5.0950	4.8230	4.1110	4.6763				
30 m LB	5.5960	5.1250	4.5580	5.0930				
120 m RB	3.4230	3.1560	3.0380	3.2057				
180 m LB	3.5180	3.3600	3.0300	3.3027				
233 m RB	2.2770	3.7460	2.0830	2.7020				
279 m LB	2.6160	2.0020	2.3760	2.3313				

Table 99 Clark's Ferry, Pool El 551.5, CHF350, Run 3 Jan 96					
		Drawdown, cm			
		Rep	olicate		
Distance from Thalweg m	A	в	с	AVG	
30 m RB	10.9020	10.2400	9.3990	10.1803	
30 m LB	11.7110	10.4150	10.2700	10.7987	
120 m RB	5.5610	5.2260	5.4830	5.4233	
180 m LB	5.5520	5.6380	5.1030	5.4310	
233 m RB	4.7990	3.6830	4.9980	4.4933	
279 m LB	4.6860	4.4510	4.1270	4.4213	

Table 100 Clark's Feri	Table 100 Clark's Ferry, Pool El 551.5, CHF376, Run 4 Jan 96					
		Drawdown, cm	l			
		Rej	plicate			
Distance from Thalweg m	A	В	с	AVG		
30 m RB	11.6300	11.4640	10.9990	11.3643		
30 m LB	12.3230	12.5590	12.2330	12.3717		
120 m RB	6.5190	6.3900	6.5650	6.4913		
180 m LB	5.6610	5.8100	5.8550	5.7753		
233 m RB	5.8400	6.0410	6.1780	6.0197		
279 m LB	5.3160	4.9630	4.7840	5.0210		

Table 101 Clark's Ferry Pool 572.7 Drawdown Experiment Conditions										
Experiment No.	Up or Down ¹	Tow Speed ² m/sec	Position ³	Temp ° C	Actual Draft m	Effective Draft⁴ m	Barge W X L	Prop Thrust 1,000 lb	Schijf Velocity⁵ cm/sec	Schijf Drawdown⁵ cm
COR260	-	2.60	268.3	9.5	2.13	2.75	3X5	81	3.4	0.9
COR350	-	3.50	268.3	9.5	2.13	2.71	3X5	108	4.7	1.7
COR376	-	3.76	268.3	9.5	2.13	2.70	3X5	135	5.2	2.0
Note: Water surface width 629.5 m, area 7,283 sq m, water surface elevation 572.7, 26° rake. ¹ Slack water. ² Relative to ground. ³ Meters from right bank. ⁴ Actual draft + draft correction. ⁵ Schijf equation using effective draft and vessel speed relative to water.										

Table 102 Clark's Ferry, Pool El 572.7, COR260, Run 27 Dec 96							
Drawdown, cm							
	Replicate						
Distance from Thalweg m	A	В	с	AVG			
30 m RB	1.7530	1.7590	1.7340	1.7487			
30 m LB	2.6660	2.1900	1.9960	2.2840			
120 m RB	1.5670	1.1840	0.7740	1.1750			
180 m LB	0.8840	1.0240	0.6330	0.8740			
233 m RB	0.4410	1.7840	1.3340	1.1863			
279 m LB	0.8690	0.8410	0.9400	0.8833			

Table 103 Clark's Ferry, Pool El 551.5, COR350, Run 28 Dec 96							
Drawdown, cm							
	Replicate						
Distance from Thalweg m	A	В	с	AVG			
30 m RB	4.3780	3.1150	2.5790	3.3573			
30 m LB	4.0850	4.0450	3.1350	3.7550			
120 m RB	1.6140	1.5500	1.8080	1.6573			
180 m LB	1.4070	1.2480	1.4470	1.3673			
233 m RB	1.4680	1.8440	1.5830	1.6317			
279 m LB	1.1400	1.3730	1.2570	1.2567			

Table 104 Clark's Ferry, Pool El 551.5, COR376, Run 29 Dec 96							
Drawdown, cm							
	Replicate						
Distance from Thalweg m	A	В	с	AVG			
30 m RB	3.0250	5.4120	3.9670	4.1347			
30 m LB	4.2600	4.8680	4.5540	4.5608			
120 m RB	2.1430	1.8870	1.5910	1.8737			
180 m LB	1.9440	2.1130	1.4870	1.8480			
233 m RB	2.0070	1.3280	1.5000	1.6117			
279 m LB	1.5760	1.1960	1.3390	1.3703			



Figure 1. Clark's Ferry site on the Mississippi River, RM 468.2



Figure 2. Cross section of the Mississippi River at the Clark's Ferry site for trip 1



Figure 3. Cross section of the Mississippi River at the Clark's Ferry site for trip 2



Figure 4. Plan view of the Clark's Ferry site for trip 1 (locations of the current meters are shown)



Figure 5. Plan view of the Clark's Ferry site on the Mississippi River for trip 2



Figure 6. Plan view of 1:30 scale model of Clark's Ferry



Figure 7. Schematic of navigation effects model



Figure 8. Tow effects flume looking downstream



Figure 9. Model M/V Benyaurd



Figure 10. Connection between tow and towing carriage



Figure 11. Photo of 2D, 3D ADV's and wave gauge



Figure 12. Acceleration of model tow



Figure 13. Depth-averaged ambient velocity distribution for Pool 546.0, Q = 690 cms



Figure 14. Trip 2 verification data, 2.74-m draft



Figure 15. Trip 2 verification data, 2.13-m draft


Figure 16. Velocity time history for *Coop Ambassador*, Probe number 832, prototype data



Figure 17. Velocity time history for *Coop Ambassador*, Probe number 832, physical model data



Figure 18. Velocity time history for *Coop Ambassador*, Probe number 151, prototype data



Figure 19. Velocity time history for *Coop Ambassador*, Probe number 151, physical model data



Figure 20. Velocity time history for *Coop Ambassador*, Probe number 834, prototype data



Figure 21. Velocity time history for *Coop Ambassador*, Probe number 834, physical model data



Figure 22. Velocity time history for *Coop Ambassador*, Probe number 1131, prototype data



Figure 23. Velocity time history for *Coop Ambassador*, Probe number 1131, physical model data



Figure 24. Velocity time history for *Coop Ambassador*, Probe number 999, prototype data



Figure 25. Velocity time history for *Coop Ambassador*, Probe number 999, physical model data



Figure 26. Cross section, experimental series 1



Figure 27. Vector plot, test LCU138C



Figure 28. Vector plot, test LCU183B



Figure 29. Vector plot, test LCU228B



Figure 30. Vector plot, test LCU273B



Figure 31. Vector plot, test LCU318A



Figure 32. Vector plot, test LCD202B



Figure 33. Vector plot, test LCD247C



Figure 34. Vector plot, test LCD292A



Figure 35. Vector plot, test LCD337A



Figure 36. Vector plot, test LCD382A



Figure 37. Vector plot, test LRU228B



Figure 38. Vector plot, test LRU318B



Figure 39. Vector plot, test LRD292A



Figure 40. Vector plot, test LRD382A



Figure 41. Vector plot, test LIU228B



Figure 42. Vector plot, test LLU318C



Figure 43. Vector plot, test LLD292C

																	NΟ	ΤE:	VELI Tail	DCIT DF	Y (CI ARRI	M∕SE □W	EC)	LOC	ATED	AT	
_	5 414.9	10.9 at		j 14.8	4 18.5 4 1		 17.8ھ_ 6.	12.2	415.1	4 14.5	1 2.1	₹8.1	4.0	3.1	2.9	5.2	2.8	2.8	8.1	4 3.4	⊲ 17.5		▲ ^{8.1}	↓	a 12.5	<u>10.9</u>	
3 6.9 36.	.7 🗲 36.4	a- 37.6 a 4	2.2 -42.	7	-43.2	:3.2 ⊲ 47	.2 4 48.2	- 41.5 ·	- 42.4 -	-43.7 .	4-36 .6	4 29.2	4 21.6	- 19.0	+ 22.0	4 23.8	₹24.9	₹ 27.9	◆30.1	← 35.4	- 38.0	4 −36.4	- 3 8.8	← 40.9 ·	4 —42.4 ◄	-42.8◄	•44
● -42.1 ● -41.	2 * 3 7.9	4- 36.2 4- 3	:9.4 ← 41.8	3 🖛 40.6 ◄	⊷43.0≁	l6.4 ≁ ~45	5.1 • - 4 4.8	*− 48.6*	 50.0 -	~ 4 8.5 `	3 9.9	* 28.6	* 22.7	₹19.2	⊲ 17.2	4 19.1	4 29.5	₄ -36.0	∢ -36.6	4 −36.0 ·	4 39.3 ·	€- 38.9	4- 38.9	4- 38.9 ·	 41.0 ◄	⊢38.2 -	- 38
4- 39.2 4- 37.	.6 🖛 35.9	* 3 7,4 * 3	86.1 ≪- 35.	5 4-38.0 4	4~3 9,3 4 ~	i2.0 4 - 43	3.0 - 4 4.8	3 ▼ -4 4.3*	4 46.2 [≪] -	4 9.5	41.2	19.1	17.0	¶15.1	4 10.2	9.8	28.1	38.7_ ہ	- 31.6.	≪ 29.4	≪ 31.4	4- 32.5	- 34.1	≁- 34.6	≪ -33.5 ◄	►33.9 •	- 35
← 33.0 ← 31.	9 -32.2	• 312 • 3	82.1 +31.4) 4 32.8 •	- 35.6 - -3	17. 3 	' .5 ∢ -40.2	4−40.0	 -44.4 - -	48.5	6.0 تر	⊿ 10.1	¶2.4	4 11.7	₹6.2	4 8.0	24.6	₹- 37.5	4- 33.9	4 -31.5	4 -32.1	- 32.6	- 32.3	4 29.5	4 29,3 ∙	•-30.2	4 18
← 30.5 ← 29.	.1 -30.0	◆ 28.9 ◆ 2	:7.0 +30.)	8 4-32.8 -	← 31.3 ▲ ←	36.2 🖛 38	8.9 4-4 2.2	2-43.8	 45.9 -	⊷ 42.0	₄- 32.1	4 18.7	₹9.4	4.8	2.3	2.9	1 1.7	* 25.5	4 -29.0	4 27.9	4 -28.6	≁ -29.2	4 27.2	4 28.8	4 29.0 •	€33.2	~ 18
◆ 21.1 ◆ 20.1	9 418.9	€21.3 €2	4.4 4 25.	3 424.5	4 23.6 4 4	25.8 -32	2.1 🕳 31.9	4 −36.0	← 37.2 ◄	4- 31.4	4 24,7	4 15.1	¶12.4	7.7	7.8	5.3	₹6.1	⊲ 18.6	4 24.6	4 23.8	4 22.0	4 22.0	4 21.6	4 22.6	4 22.3 ·	4 24.3	42.
4 26.2 4 27.	1 424.8	4 22.9 4 2	4.3 424.	3 424.9	4 23.6 4 7	26.5 🛶 30	0.7 🛥 35.7	′ 4 -36.5	4- 33.8 ▲	← 31.3	4 25.9	4 18.2	₹11.6	▲ 5.5	4	1.5	▲ ^{8.3}	4 19.2	4 24.7	€ 24.0	4 22.3	4 22.5	4 23.5	4 23.6	423. 3	4 23.9	4 3.
-9	-8	-7	-6	-5	j -	-4	-3	DIS.	r 2 Tanc	т -1 СЕ	FRП	0 M F	30V.	1 M	2 2 /10	10	3		Г 4	5		6		7	8		9
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Figure 44. Vector plot, test LLD382C



Figure 45. Vector plot, test LCUU22B



Figure 46. Vector plot, test LCUU31A



Figure 47. Vector plot, test LCUU40B



Figure 48. Vector plot, test LCUD29A



Figure 49. Vector plot, test LCUD38A



Figure 50. Vector plot, test LCUD47C



Figure 51. Vector plot, test LC1U29B



Figure 52. Vector plot, test LC1U31C



Figure 53. Vector plot, test LC1D29C



Figure 54. Vector plot, test LC1D38A



Figure 55. Vector plot, test LC2U22A



Figure 56. Vector plot, test LC2U31B


Figure 57. Vector plot, test LC2D29B



Figure 58. Vector plot, test LC2D38A



Figure 59. Vector plot, test LC3U22B



Figure 60. Vector plot, test LC3U31B



Figure 61. Vector plot, test LC3D29A



Figure 62. Vector plot, test LC3D38B



Figure 63. Vector plot, test LC4U22C



Figure 64. Vector plot, test LC4U31B



Figure 65. Vector plot, test LC4D29A



Figure 66. Vector plot, test LC4D38C



Figure 67. Return velocity, tow length effects, upbound tow



Figure 68. Return velocity, tow length effects, downbound tow



Figure 69. Drawdown versus tow length, tow speed relative to water = 2.6 m/sec



Figure 70. Drawdown versus tow length, tow speed relative to water = 3.5 m/sec



Figure 71. Vector plot, test LCEU22C



Figure 72. Vector plot, test LCEU31C



Figure 73. Vector plot, test LCED29B



Figure 74. Vector plot, test LCED38C



Figure 75. Return velocity, rake angle effects, downbound tow



Figure 76. Return velocity, rake angle effects, upbound tow



Figure 77. Cross section, experimental series 5



Figure 78. Ambient velocity distribution, experimental series 5



Figure 79. Vector plot, test HCD202



Figure 80. Vector plot, test HCD247



Figure 81. Vector plot, test HCD292



Figure 82. Vector plot, Test HCD337



Figure 83. Vector plot, test HCD382



Figure 84. Vector plot, test HCD477



Figure 85. Vector plot, test HCU138



Figure 86. Vector plot, test HCU183



Figure 87. Vector plot, test HCU228



Figure 88. Vector plot, test HCU273



Figure 89. Vector plot, test HCU318



Figure 90. Vector plot, test HCU416



Figure 91. Plan view, experimental series 6



Figure 92. Comparison of experiments in experimental series 6


Figure 93.Velocity time history, upbound tow, meter No. 3, tow speed relative to ground = 4.16 m/sec



Figure 94. Velocity time history, upbound tow, meter No. 4, tow speed relative to ground = 4.16 m/sec



Figure 95. Velocity time history, downbound tow, meter No. 3, tow speed relative to ground = 4.77 m/sec



Figure 96. Velocity time history, downbound tow, meter No. 4, tow speed relative to ground = 4.77 m/sec



Figure 97. Location of velocity meters in dike experiments







Figure 99. Profile of high (generic) dike (looking upstream)



Figure 100. Experimental series 6, downbound runs (Continued)



Figure 100. (Concluded)



Figure 101. Experimental series 6, upbound runs (Continued)



Figure 101. (Concluded)



Figure 102. Velocities during tow passage, low dike, downbound tow (Continued)



Figure 102. (Concluded)



Figure 103. Velocities during tow passage, low dike, upbound tow (Continued)



Figure 103. (Concluded)



Figure 104. Velocities during tow passage, high dike, downbound tow (Continued)



Figure 104. (Concluded)



Figure 105. Velocities during tow passage, high dike, upbound tow (Continued)



Figure 105. (Concluded)



Figure 106. Cross section, experimental series 7

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-16.0	4 14.7	4 14.8	+ 13.6	4 15.0	~ 14.1	4 13.8	4 12.4	4 13.5	4 15.9	4 11.1	₹9.4	▲ 8.0	▲ 10.4	▲ 9.1	▲ 9.0	∢ 9.8	4 10.2	_ 11.5	4 12.3	4 13.3	4 12.4	4 12.7	▲ 9.4	▲8.9	₹9.3	a 11.4	- 12.4	_ 10.7	₹7.1	≼ 4.8
26.0	4 -21.5	4- 23.2	4- 22.6	4 -20.3	← 18.0	- 21.8	4 -20.2	< -26.7	₹20.5	₹17.4	≁- 21.9	- 17.4	₹ -18.4	≁ 26.1	4 -21.3	≁ ~21.9	4 -21.3	4 -22.5	4 -26.2	₹19.5	4 26.7	4- 27.9	4 2 2.2	4 26.4	4- 22.4	4 -20.9	← 19.5	- 27.1	* 13.4	◄10.5
+15.8 ₹ 18.3	◆ 16.2 ◆ 13.7	4 20.4 ₹ 19.3	4- 22.5 ▲ ^{24.4}	€ 23.6 € 17.6	 4-23.5 ₹ 20.3 	 4 22.0 16.4 	←21.5 ▼14.4	- -22.0 + 17.5	 4 20.4 19.5 	4 -19.5 ₹ 14.6	 414.5 ↓ 17.9 	+15.9↓13.3	 ◆16.3 ▶ 14.5 	4-16.112.4	▲14.9 ▲ 13.9	21.1 23.3	-21.5 ⊐ 20.2	←24.1 ▼ 21.1	 € 20.3 	- 20.2 ▼ 22.4	 20.9 - 18.5	21.7 24.1	24.0 19.8	26.9 €11.8	- 24.8. * 12.9	▲-24.9 ▲-24.9	 €-23.9 €-22.2 	 27.9 ■14.1	- 19.3 ▲ ^{16.0}	 ▲14.9 ▲16.0
k 15.8	4 -18.4	4- 18.9	19.6	19.1	▲19.0	₹15,6	1 3.3	4 -18.5	£2.0	₹ 18.0	R 15.3	12.9	k 15.9	▼ 11.4	† 19.1	4 -19.1	₹16.1	¥ 16.0	≁ 16.6	₹ 14.8	4 -19.0	1 6.9	* 16.0	17.2	◆ 17.2	- 18.4	21.1 م ر	19.8ھ	4 7.5	4 7.5
-15.5	◆ 16.5	← 17.7	4 16.8	4 17.8	←1 7.1	4 16.2	⊄ 15.1	4 -16.6	< 16.6	4 15.9	← 13.4	∢ 12.7	4 14.9	4 13.9	◆ 13.7	← 15.8	4 14.4	4 15.2	← 17.8	4 15.6	◆ 15.5	← 15.8	* 15.1	← 15.4	≁ 16.0	◆ 14.1	← 16.4	* 14.9	⊲ 7.4	▲ 7.4
∎10.0	∢ 9.2	4 11.7	₹6.8	₹7.2	∢ 6.5	▲ 8.7	4 7.4	⊲ 8.8	₹9.5	₹5.1	4 8.3	4 12.2	∢ 8.7	∢ 9.8	4 10.3	∢ 10.8	₹11.5	◄10.1	⊲7 .7	⊲ 10.3	← 17.5	▲ 13.4	4 12.3	◄ 9.1	+ 12.8	⊲ 10.5	⊲ 10.7	◆13.1	∢ 7.3	₹7.3
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																							\lor	ΈL	- [] (TE	CIT St	Ү СН	D52	IC T 92	٦DR

Figure 107. Vector plot, test CHD292



Figure 108. Vector plot, test CHD382



Figure 109. Vector plot, test CHE472

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25.7 +29.7 +25.2 +2 40.0 *27.4 *28.4 *2	24.6 2 2.9 4	30.5 -31.1	← 33.6 ← 36.1 ← 31.4 ← 30.1	7 - 30,6 - 5 - 28.6 -	29.7 ~ 21.8 31.3 ~ 24.3	+21.4 + +29.5	 €28.0 €28.3 €28.3 €28.3 €28.0 €28.0	• • • • • • • • • • • • • • • • • • •	9 - -30.0 - € .8 - 23.3 - € 7 \ 31.4 2	24.5 ~2 5 29.6 3 0.1	.5 < 2 5.5 < 6 30.7	-27.4 + 125.7 + -33.5	25.6 - 26.	8 4 25.7 · 1 1 2 43.8	←27.6 ← 42.6	-27.7 +	28,4 - 27,5 28,4 - 30,5 32,9 [•] 34,5	3 - 31.4 • 3 - 31.4 • 3 - 31.3	⊷31. ₹ 32.9
-30.2 -32.2 -33.4 -3	32.1 * 37.6	44.4-44.4*	[⊷] 41.8 ^{≪46.}	4	40.2 4 4 0.7	★39.4 ★	-39.4 -39.4	· * 39,0 * 38	.3 - 38.6 -	39.5 40.	.6 🕶 41.1 🔻	37.9 •	`a≥ 2 * -36.	7 38.2	* -33.6 *	-38.4 🔦	32.0 -33.5	5 * 33 .5 *	33:
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Figure 110. Vector plot, test CHU228

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28.4	≠ 25.4	* 25.1	₹ 27.1	₹ 27.2	◆28.4	4 26.9	₹28.0	₹26.5	₹23.2	* 20.3	₹21.1	4 20.8	4 18.9	* 20.5	₹ 20.5	4 18.2	₹21.4	4 20.3	* 21.9	* 23.5	₹20.6	₹ 23.9	₹ 21.9	* 22.7	₹19.1	₹ 21.9	₹21.6	* 21.5	⊲ 17.7	₹19.3
31.2	◆ 28.5	4 26.0	4 28.3	4- 32.4	4- 35.2	4 3 6.5	4- 32.7	4- 33.0	4 -32.8	~ 28.1	≁ 26.0	≁ 28.2	≁ -28.1	₹ 27.4	₹26.9	* 27.8	4 26.3	₹29.7	₹ 28.9	≁ 30.5	4- 32.3	➡30.1	←30.1	₹30.3	≁ -29.1	≁ -30.3	₹30.0	₹33.0	₹32.5	≁ -34.4
28.5	4 28.8	≠ 26.0	4 24.3	4 25.7	- 30.7	4 -30.0	428.4	₹-30.6	₹ 30.8	₹ <u>27.9</u>	22.3	₹ 28.4	4 27.7	₹ 26.6	₹29.2	4 29.7	₹ 29.5	€ 29.9	◆ 29.9	* 28.7	₹27.8	* 27.1	4 26.7	4 -28.1	← 28.0	4 27.7	4 27.5	◆ 28.0	₹27.0	₹25.6
2.6	4 23.3	18.9	k 27.3	1 29.6	₩27.7	4 29.2	39.4	₹24.6	24.0	41.9	€ 20.0	№ 20.3	₹22.6	₹23.0	\$ 22.6	23.1	* 19.7	* 19.5	▲ ^{37.8}	4 26.9	x 23.2	20.8	▲ ^{34.9}	4 ^{33.6}	21.2	* 22.9	23.4	20.6	₹ 29.4	▶ 24.0
7.7	₹17.1	1 6.8	16.3	k 23.5	21.7	20.6	18.5	18.5	€ 20.6	4 17,6	15.9	► 15.7	¶ 4.7	₹15.0	₹15.3	4 18.4	¶ 3.3	₹13.8	₹14.1	1 3.3	1 2.2	1 3.7	₹13.8	₹15.2	⊲ 19.5	4 17.3	11.4	₹11.4	13.5	14.6
5.2	₹3.4	₹2.6	₹2.8	¶4.2	₹15.2	4 4.4	4 4.7	◄14.1	⊲14.1	◄12.1	4 12.8	⊲11.6	⊲ 11.3	4 10.9	⊲ 11.9	⊲ 12.1	◄9.8	◄11.4	◄11.1	∢ 11.1	4 0.9	⊲ 9.9	∢9.6	⊲ 10.8	₹10.9	⊲ 11.9	⊲ 10.9	⊲1 0.6	4 10.2	⊲ 11.1
5.6	⊲ 12.1	4 9.3	4 8.7	⊲ 9.5	₹10.2	₹7.0	₹4.9	4 9.7	∢ 3.4	₹2.9	⊲ 9.9	⊲]].4	4 11.1	₹2.8	⊲ 4.8	₹3.5	⊲ 8.6	₹12.0	₹3.3	◄11.8	₹5.3	⊲ 8,4	₹10.2	⊲ 9.2	₹7.0	4 6.7	₹5,9	₹8.0	⊲ 9.8	⊲ 8.2
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Figure 111. Vector plot, test CHU318



Figure 112. Vector plot, test CHU408

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A 1:30-scale model of the velocity and drawdown. The prototype data from the Clark tow positions, vessel speeds, of uniform, except near the bed. return velocity. Velocity mean model was used with a large of	e Missis model w c's Ferry : drafts, ar Rake ar asuremen depth to s	sippi River near Clark's l as adjusted to account for reach. Return velocity and d direction relative to flor agle at the bow of the vest ts near submerged dikes simulate open river conditional to the the test simulate open river conditional to the test of the test of the test simulate open river conditional to the test of t	Ferry, Iowa, was used t r scale effects based on ad drawdown were deta ow. The vertical profil sel of 26 deg and 45 da were documented durin tions below St. Louis.	to determir n a compar ermined fo e of return eg was sho ng vessel p	the tow-induced return ison of physical model and r various pool elevations, velocity was shown to be wn to produce similar bassage. The Clark's Ferry	
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